REPORT ON SOIL INVESTIGATION AND RECOMMENDATION ON FOUNDATION FOR THE CONSTRUCTION OF STILT+8 STOREYED MIG FLATS AT ZONE 'M2' OF PERUMBAKKAM PROJECT

Job No: SF/KI-48/ Perumbakkam/Zone 'M2'/TNSCB/2013

Client: The Executive Engineer, ETRP (C-II) Division, TNSCB Semmenchery, Chennai-600 119.

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1. Introduction

The Executive Engineer, ETRP (C II) Division of TNSCB has sent a request to conduct soil investigation in their housing project site at Perumbakkam TNSCB scheme area through Lr.No:203/E.C/ETRP CII/2012, dt: 03.01.2013 for the construction of MIG and FIG Flats. The Board proposed to construct residential flats in their housing scheme area as detailed below:

Sl.No	Detail	Number of blocks	Area of each unit (m²)	Number of units
1.	MIG Flats (Stilt + 8 Floors)	12 (64 units in block each)	73.9	768
2.	FIG Flats (Stilt + 8 Floors)	4 (64 units in each block)	97.3	256

To construct these residential blocks an area of 7.13 Hectares is allotted covering survey Nos: 539/2, 540/1, 540/2 and part of 537. The area earmarked for the said purpose is shown in key map (Fig.1a) of the TNSCB Perumbakkam scheme. The proposal of the Board comprises of building nine storeyed (Stilt + 8 floors) framed structures. The Perumbakkam village is located at a distance of about a kilometer



towards western direction from OMR. A road of 18m wide is connecting this village with OMR. On the Southern side of this road and adjacent to existing TNSCB scheme at Semmencherry, the Executive Engineer (Div VI) of TNSCB executed similar project over an area of 30 Acres covering S.Nos: 542 to 544 during 2009. At this area eight storied framed structures were constructed and they are ready for occupation. These buildings are supported on raft foundation and the depth of foundation of all the buildings is around 4m. The Fig A1 shows the land allotted for the proposed construction including the area where project is completed.

On allocation of land by the Government The Executive Engineer (Div.II), TNSCB took initiative to implement the project and requested the services of Department of Civil Engineering to conduct Soil Investigation for the construction of Block 12 to 18 (S.No: 528) and constructions of Blocks covering area coming under S.Nos:479/2 and 482 to 485. These two locations are marked as Zone 'A 'and Zone 'B' in layout plan (Fig A1) and they lie in the south and north west part of the land allotted for the project.

At Zone 'A' investigation was conducted at 5 locations during April 2010. The top layer is expansive clay of 1.5m thick followed by clayey sand of 1m. Weathered rock was met at the depth of 2.75m invariably and fairly good rock was seen at depth around 4m. The water table was met at the depth of 2.5m. Based on the soil condition of the area, it was recommended to adopt raft foundation at the minimum depth of foundation of 3m (RL -1.45m).

At Zone 'B' investigation was carried out during the second week of June 2010 by drilling eight boreholes. The deposit of this area composed of highly plastic clay of 2m to 2.7m thick followed by residual soil (weathered rock reduced to soil) of 1m to 1.5m thick. However the deposit below 4.5m was fractured rock. At this area the water table was at the depth of 3m. The foundation recommended for the eight storeyed structures was raft foundation and minimum depth of foundation was 2.75m (i.e. RL -1.35m) from the lowest ground level. Recommended bearing capacity was 200kN/m². The board commenced the construction work at Zone 'A' and 'B' in the second week of May 2012.

In the remaining part of allotted land of Perumbakkam village, the Executive Engineer, JNNURM Division sent a request through Lr.No:171/JNNURM Dn/A1/2011, dt:28.3.2012 to inspect and conduct subsurface investigation covering survey nos: 509,510,511,516,517,518,536,537 & 538 for the construction of eight storeyed residential block in these location. Accordingly investigation was conducted at 40 locations covering 125 acres of land. Since the area was large, it was divided conveniently in to Zone 'C', Zone 'D', Zone 'E' and Zone 'F' as indicated in Fig A1.

The sub-surface investigation in all these areas was commenced on 25th April 2012 and completed on 19th May 2012. The report was released for each zone independently. The recommended foundation was raft for the eight storeyed buildings irrespective of the Zones in which buildings are proposed to locate. The recommended depth of foundation at different Zones is as below:

Zone	RL of Foundation (m)	Bearing capacity
С	between - 1.0m and -1.2m	220kN/m ²
D	between 1.9m and -2.6m	220kN/m ²
E	between 1.1m and -1.6m	220kN/m ²
F	between - 0.9m and -1.2m	220kN/m ²

Foundations of buildings were located at depths as recommended without difficulty except one or two blocks. As stated in the first paragraph of the report the board has drawn a proposal to construct MIG and HIG Flats in this area for the public, since the area lies within a distance of 2km from OMR and demand for house is more in this area.

The board has earmarked the area for this proposal, which lies in the south east part of the Perumbakkam scheme, which is about 7.13 Hectares. The project site was inspected along with the Executive Engineer of ETRP Division and other officials on 28.02.2013. Since the project area is large (total extent is 7.13 Hectares) the buildings are nine storeyed framed structure and this area comes under zone III as per IS1893-2002(Part-1), it is decided to investigate over entire area covering all the 16 blocks. At the end of investigation it is proposed to explore at two locations for each MIG block and at three locations for each HIG block. This proposal is been accepted by the Executive Engineer.

Accordingly locations of boreholes for each block were selected and mutually agreed to investigate at 36 locations as detailed below:

Zone	Number of Blocks	Boreholes
M1	M1 to M6	BH1 to BH12
M2	M7 to M12	BH13 to BH24
Н	H1 to H4	BH1 to BH12

Since large part of Perumbakkam Housing Project area was covered in earlier investigation and over all soil condition of this area is known to consultant. In this area, the hard stratum with good bearing resistance occurs within a depth of 4.5m; therefore it is felt sufficient to investigate to a depth of 9m. However one or two boreholes were drilled beyond the depth of 9m to know relative degree of weathering of rock deposit and its quality. The soil investigation work in all the three zones is commenced on 04.03.2013 simultaneously and completed on 9.4.2014.

2. Details of the project

The project to be executed in this area is construction of multi-storeyed blocks for the middle and high income group people under Rajiv Awas Yojana scheme. In this project the Board is proposed to construct 9 storeyed (Stilt + 8 Floors) framed structure by adopting two different type design; one is for MIG and the other is for HIG. Apart from construction of residential buildings they develop other amenities like club house, Gym, Park etc. However the soil investigation carried out is found mainly for the construction of multi-storeyed buildings. Each block of MIG is designed to accommodate eight families in each floor with plinth area of 73.9m²/ family. Similarly the HIG flats are also designed to accommodate eight families in a block with plinth area of 97.3m²/unit.

The structure is nine storeyed building and the area of construction is located within 20km distance from Chennai. The Chennai and its neighboring areas is coming under Zone III, hence the structure of this area is to be designed for Zone III conditions. Moreover in the recent past Chennai has experienced mild tremors and the earthquakes occurred in Sumatra islands and Pondicherry coast also felt in some parts of Chennai.



Therefore the board has analyzed the building for the Zone III condition. The minimum and maximum load at the foundation level for the critical load combination was reported as 869kN and 1890kN respectively. Since the soil is in the heterogeneous condition and in hard layer (i.e. weathered rock) clay lumps are seen during investigation, which is not conducive for isolated footing. Therefore the average load at the foundation level for the raft was obtained for the critical combination of load, which is 219kN/m².

3. Preliminary Inspection of the project area

Perumbakkam area has experienced fast development within a period of four years. The land of Perumbakkam area covering survey numbers as per the key plan (Fig. 1a) was occupied by the local people of the area. This entire area was covered with thatched roof houses, semi permanent and permanent buildings. The local town Panchayat laid temporary roads and provided water and power connections to the houses. Certain houses were provided with soak pits and were connected to toilets. These soak pits are 3.5 to 4m deep from the existing ground level. The area identified for the development of project is covered by 18m road on the south, compound wall of Bollini Hill Housing complex on the west, open private land on north and proposed PWD Drain of 40m wide on the east. This area is at a distance of approximately 2km from the OMR. The ground level of this area though it appears uniform, it is slopping from west to north east direction. The construction of multi-storeyed buildings in this project area was commenced during 2010 in Zone A and covered most part of the area part by part. The part of land, on the south east side of the area covering S.Nos: 537, 539/2, 540/1, 504/2, 541 is vacant and is been identified for the construction of multi-storeyed flats. This area lies within the boundary of 18m wide Semencherry-Perumbakkam road on the south; 30m wide road and PWD drain are on the east, Zone D on north and community facilities of Zone A on the west. The total area is 71330m². The ground level of this area is almost uniform and is also free from shrubs and old structures; hence the site is ready for soil investigation. There is a mountain at a distance of about a kilometer or more on the western side and the ground is slopping from the foot of the hill towards east. At the



proposed construction site the ground level is the lowest while comparing with the ground level of neighboring areas. This area is prone for water logging hence the board is proposed to raise the existing ground level.

As stated in the introduction, the area of Perumbakkam (Zone A to Zone F) was already investigated at different pint of time for the purpose of locating suitable depth for foundation of eight storeyed structures and reported occurrence of hard stratum invariably at the depth below 4.5m and the weathered residual soil at depth of around 2.75m. The weathered residual soil was in hard/dense condition with N values more than 50 blows. However on the east and north east part of the area (Zone D) the deposit over a depth of 3m is soft. Keeping this in mind, it is proposed to investigate up to the depth of occurrence of hard stratum (N>100) at all the 36 boreholes. In a few boreholes rock drilling using single tube core barrel with diamond cutter is also recommended in order to confirm the presence of true hard stratum to a reasonable depth. The officials of TNSCB have agreed for this suggestion and proceeded accordingly.

Since the soil condition at major part of Perumbakkam project area is known from the earlier subsurface investigation carried out for the blocks at Zone 'A' to zone 'F' it is agreed mutually by the consultant and the officials of TNSCB to restrict the number of investigation points as minimum as possible. Since buildings are located as clusters accommodating other amenities for each cluster, it is decided to group at each cluster as individual zone. Thus there are three zones (M1,M2&H) and is mutually agreed to investigate at 12 points in each zone by distributing minimum of two exploratory points for each block. The subsurface investigation at the proposed construction area was commenced during the fourth week of February 2013. At all the borehole locations, the borehole was advanced using rotary drilling technique and standard penetration tests were conducted in each borehole at spacing of 0.75m using standard split spoon without liner as per IS2731-1972. The subsurface investigation work in this area was executed by M/s. Geotechnical solutions, Chennai under my (Prof.K.Ilamparuthi, Professor and Chairman, Faculty of Civil Engineering) supervision. This report presents salient details of

investigation and soil type encountered along with recommendation on foundation for the Zone M2.

4. Site condition

The topography of Zone 'M2' is almost uniform and if at all any difference in the levels within the area of investigation may not be more than 0.5m. The deposit on the surface exhibited honey comb pattern tension cracks, which confirm that the top soil is dominantly clay with shrink and swelling quality. Further there is a mountain at a distance about a kilometer or more from the western boundary of proposed construction area. It provides the clue that the rocky stratum will be at a shallow depth in the construction area and the soil cover that lies above is certainly residual deposit. However there is a chance for transported soil deposit on the surface since the ground is slopping from mountain on the west to canal on the east and the ground level is lower in this zone.

5. Details of soil investigation

At Zone 'M2' soil investigation was carried out at 12 locations as shown in Fig.1b. It can also be seen that the locations of various blocks. The details of borehole locations and the ground level at each location are presented below:

Bore hole No	Identifi cation	Location	Ground level (RL)	Water Table (RL)
1	BH13	Block M7	+1.688m	+0.288m
2	BH14	Block M7	+1.415m	+0.051m
3	BH15	Block M8	+1.339m	+0.039m
4	BH16	Block M8	+1.240m	+0.140m
5	BH17	Block M9	+1.492m	+0.092m
6	BH18	Block M9	+1.409m	+0.009m
7	BH19	Block M10	+1.409m	+0.109m
8	BH20	Block M10	+1.250m	+0.150m
9	BH21	Block M11	+1.354m	+0.154m
10	BH22	Block M11	+1.267m	+0.267m
11	BH23	Block M12	+1.200m	+0.200m
12	BH24	Block M12	+1.295m	+0.295m



The boreholes were made to collect information on nature of overburden and depth of occurrence of hard stratum. They were drilled using rotary method with bentonite mud circulation. This method is normally adopted to advance the boreholes both in residual and sedimentary deposit. The circulation of drilling fluid was employed through drill rods and letting out through the jets provided in the cutting tool. The jetting action with pressure flow brings the cut material to the surface through the annular space between the sides of boreholes and drill rod. Boreholes of diameter 150mm were drilled by adopting this method. During drilling it was ensured that the borehole was kept full with drilling fluid to avoid disturbance to the sides as well as bottom heave. In the boreholes, standard penetration tests were conducted at required depth or wherever there was a change in the soil layer. This test was conducted using standard dimension split spoon without liner as per the procedure given in IS 2731-1972 using donut type hammer dropped mechanically (2 turns of rope in the cathead arrangement). The energy of impact was around 70%. Thus the field value was N₇₀. However the filed N values were corrected for the installation procedure and the value was very close to N₆₀. Therefore recorded values were taken as N₆₀. The values thus recorded were not corrected for overburden since the top soil to the depth of 2.5m was having fines more than 50%. Further the correction for saturation was also not applied for the resistance values recorded below water table since the deposit was not fine sand. Further the overburden correction factor is greater than unity for the N values recorded at shallow depths; hence the said conditions will certainly result in conservative resistance of deposit. The soil samples obtained from the split spoon were visually identified and tested in the laboratory for assessing index properties. Soil samples collected in split spoon samplers are subjected to test for index properties. The boring and sampling operations were continued at each location until refusal N value (rebound) was recorded or two consecutive N values were grater then 50 blows and the third N value was more than 100 blows. However at locations wherever rock was encountered, exploration was continued using single tube core barrel with diamond cutter. In the rock stratum drilling was done to a depth not less than 1m and obtained core samples. In all the boreholes level of water table was recorded. The depth of VII Engg.

ground water table recorded at various locations is included in the table presented in this section.

6. Soil profile of the proposed site

The investigation at this area was commenced after marking borehole locations and their reduced levels. The reduced levels of borehole locations are almost uniform at most of the locations except at BH13 and BH23. The difference in level is 0.5m between BH13 and BH23 and the RL at BH13 is ± 1.688 m. As stated in the previous section, the soil profile is logged at each location based on soil samples obtained using split spoon sampler. The profiles thus logged at 12 locations are presented in Figs 2 to 13 along with N values recorded. The field N values recorded are taken as $(N_1)_{60}$ (i.e. design N values) for the reasons already stated irrespective of the depth and nature of deposit of this area.

The disturbed samples of each borehole are tested for index properties inclusive of swell quality. The index properties such as Gradation, Atterberg limits, and Free Swell Index are presented in Table 1 to 12 for the boreholes BH13 to BH24. The gradation curves are presented in Annexure G. The undisturbed samples obtained from the clay layers are tested for strength. The strength is determined from the samples by conducting unconsolidated undrained test at their natural moisture contents and the respective stress-strain responses are present in Annexure-U along with Mohr-Coulomb envelope. The strength and secant modulus are also presented. The compressibility properties of clay deposits are determined from index properties using established empirical equations. The soil deposits logged at each block are presented and discussed below.

Block M7

The block M7 is located on the northwest corner of the Zone M2. At the block M7 two exploratory boreholes (BH13&BH14) were made by locating them diagonally opposite to each other in the northwest and southeast corners of the block. At these two boreholes exploration was done to a depth of 8.3m and 8.7m respectively and the borehole were terminated in severely jointed rock.



The difference in ground level at both the borehole locations is about 0.2m, which shows that the terrain is almost uniform at Block M7. The soil profile logged at BH13 and BH14 is presented in Fig 2 and 3 respectively along with N values recorded.

At BH13 the top layer to a depth of 1.9m is silty clay. This layer recorded a minimum N value of 10 blows at the depth of 0.75m and a maximum value of 25 blows at the depth of 1.5m. This clay layer is in medium stiff to stiff condition and its stiffness is increased with depth. Results of Atterberg limit tests and free swell index show that this layer is high plastic clay (CH) and it possess volume change quality. Its liquid limit and plasticity index are more than 67% and 43% respectively. The deposit between the depth of 1.9m and 5.5m is a residual deposit. In this residual deposit, clay content is about 20% and is classified as SC/SM. This intermediate layer is in dense condition and becomes very dense layer by recording N value > 100 blows. The rock is encountered at the depth of 5.5m, which is highly weathered and further exploration to depth of 8.3m confirms that the rock deposit is becoming strong. However the deposit at the depth of termination is severely jointed with core recovery ratio of 13%, which can be seen from the plate 1 wherein core sample obtain between the depth 7.3m and 8.3, is shown. Thus the deposit at BH13 within the depth of investigation of 8.3m is three layer system comprises of top layer of high plastic clay (CH), intermediate residual deposit of clayey sand (SC/SM) followed by weathered rock.

The BH14 which is been made at the southeast corner of block M7 has also recorded identical soil condition (three layer system) as that of BH13. The top soil to a depth of 2.2m is silty clay. This layer is in medium stiff condition at the depth of 0.75m and is becoming stiff at depth 1.5m. This layer contains plastic clay which is known from the plastic index values of the clay (I_p>61%). Its free swell index values are also more than 67% (Table 2). Thus the soil is clay of high plastic (CH) and is susceptible for volume change. The layer that follows the clay is clayey sand/silty sand with fines in the range of 15% to 30%. The N values recorded in this layer are between 25 and 100 blows, indicating that the layer is dense to vary dense condition. The deposit that lies below the depth of 5.0m is weathered rock; its degree of weathering appears to be the same, which

is known from the recovery ratio of core samples. The recovery ratio of rock core between the depth of 5.0m and 8.7m is between 8% and 15% with nil RQD.

Block M8

The Block M8 is located on the southern side of Block M7. In the location of Block M8 two boreholes (BH15&BH16) were made as shown in Fig.1b. BH15 was made on the northwest corner whereas BH16 was made at the southeast corner of the block. At BH15 exploration was terminated at the depth of 7.6m whereas BH16 was terminated at the depth of 10.2m from the respective ground levels. The ground levels at BH15 and BH16 are +1.339m and +1.24m respectively. The soil profile logged and N values recorded at these two borehole locations are presented in Figs 4&5.

At these two borehole locations top soil to a depth of 2m is silty clay with N values in the range between 8 and 21 blows. The silty clay layer is medium stiff at the depth 0.75m and becomes stiff at 1.5m. Its index test results are presented in Table 3 and 4. It has high liquid limit (between 62% and 88%) and plasticity index values between 43% and 65%, which indicates that the fines of this layer is plastic and the soil is classified as clay of high plastic (CH). The layer that lies below the silty clay layer is clayey sand/silty sand with fines less than 22%. Thickness of this layer is about 1.5m and 2.6m at BH15 and BH16 respectively and is in dense (N>41) to very dense condition (N>100). The weathered rock that lies below residual sand layer is highly weathered and fractured. However the presence of strong layer is confirmed by drilling to a depth of 7.6m at BH15 and 10.2m at BH16. At which depths the deposits are jointed fractured rock. However at BH16 the fractured rock between 8.1m and 9.2m is highly weathered and reduced to fractions of sand and stones. Despite high degree of weathering the deposit is strong (N>100).

Block M9

At Block M9 also exploration was conducted at two locations by locating the boreholes diagonally opposite to each other. The soil profile logged at BH17 and BH18 are presented in Fig 6&7 respectively. The test results conducted on samples of split spoon are presented in Table 5 and 6.

Top layer is silty clay and its thickness is approximately 2.3m at BH17. In this clay layer liquid limit value is more than 58% and FSI values are also more than 55%. These values confirm that the clay layer is active and is susceptible for volume change due to seasonal moisture variation. The N values recorded show that the clay layer is in very soft condition (N=0). However at BH18 the top clay layer is soft to medium stiff with maximum N value of 8 blows.

The deposit between the depth 2m and 4.5m is residual clayer sand layer with fines between 12% and 25% at BH18. This layer is in medium dense (N=24) to very dense condition. The maximum N value recorded in this layer is 187 blows (extrapolated value) at 3.75m at BH18, which indicates that the stratum is becoming strong. At these two borehole locations weathered rock layer is met at depth approximately 4.5m and presence of rock deposit is confirmed by drilling to an additional depth of 3m. The borehole was terminated at the depth of 9.0m and 8.5m at BH17 and BH18 respectively, at which the rock is silt stone, which is weathered and jointed. The recovery ratio of core samples at the depth of 7.5m is 22%. The RQD of sample is zero. Plate 2 presents the core samples of BH17 and BH18.

Block M10

The Block M10 is located on the south side of Block M9 and at the location of the Block M10 exploration was done by drilling at two points (BH19&BH20) within the area of the block. The borehole 19 (BH19) is drilled at the northeast part of the block whereas borehole 20 (BH20) is drilled at the southwest part. The soil profile logged at both the locations is presented in Figs 8 and 9 along with N values recorded. At BH19 the top soil to a depth of 2.4m is silty clay, which is in soft condition ($N \le 2$). The deposit that follows the clay is silty sand of 1.6m thick between the depth of 2.4 and 4.0m. This sand deposit is in dense condition with N values greater than 44 blows. Weathered rock changes to strong (hard) rock at the depth of 6.7m and the core sample obtained between the depth of 6.5m and 7.5m recorded the recovery ratio of 31% and RQD of 28%. These values confirm that the rock occurring at depth below 7m is hard and is classified as stilt stone. The core recovered at depth below 6.5m is shown in plate.2.



The laboratory test results of samples of clay layer and clayey sand layer are presented in Table 7. The liquid and plastic limits of clay are in the range between 42% and 65% and 13% and 20% respectively. The samples also recorded FSI values more than 70%. Thus clay fines are active and plastic and the soil is classified as clay of high and intermediate plastic (CH and CI). In the silty sand fines are in the range of 14% to 16% and sand fractions are more than 80%. Thus classified as poorly graded sand / silty sand (SP/SM).

The deposits encountered at BH20 are marginally different from BH19, though the overall condition of the deposits is almost identical. The top layer is clay of high plastic (Table 8) as seen at BH19, but its thickness is 2.2m. However the clay layer has almost identical character as that seen in the clay of BH19. The second layer is clayey sand/silty sand, its thickness is about 1.2m and is in medium dense condition at the depth of 2.4m and in dense condition (N>100) at the depth of 3m. The deposit that follows the sand layer is weathered fractured rock and recorded refusal N value at the depth of 3.75m. This stratum continues up to 6.8m, at which depth, the borehole was terminated. The rock deposit available at depth between 3.75m and 6.8m is strong and less weathered since recovery ratio and RQD values are 25% and 25% respectively.

Block M11

Borehole 21 and 22 are made at Block M11 which is located almost at the centre of Zone M2. At BH21 exploration was made to a depth of 8.5m and was terminated in weathered and closely jointed rock. The deposit at this borehole location comprises of soft clay layer of 1.9m thick followed by stiff clayey sand layer of 0.4m thick. The N value recorded in the clay layer is between 2 and 7 blows. In the sand layer the resistance is high (N>44) and recorded refusal condition at the depth of 4.5. The weathered rock that follows the sand is highly weathered and it belongs to silt stone group wherein recovery ratio is between 17% and 19% in the layer between the depth of 5.5m and 8.5m. However the RQD of core samples is zero.

The soil profile logged at BH22 (Fig.11) is almost identical to that of BH21. Top layer is soft clay of 2.6m thick with N value less than 3. This layer is underlain by



organic sandy clay of 0.8m thick with N value zero. However deposit is becoming strong from the depth of 3.4m which is a fine to medium sand. Thickness of this layer is 2.2m and its coarse fraction increases with depth and also becoming very strong by recording N value >100. It is certainly a residual deposit containing weathered stone pieces. The refusal condition is encountered at 5.5m depth where the deposit is highly weathered rock. This layer continues up to 9.7m at which depth the borehole was terminated. The core samples extracted at various depths of this borehole recorded minimum core recovery of zero and maximum core recovery of 19%. The rock available between the depth 6.7m and 8.7m is weak whereas at depth between 8.7m and 9.7m is moderately strong. However the deposit below the depth of 5.5m can be considered as strong bearing layer. The laboratory test results of top clay layer of BH21 and BH22 are presented in Table 9 and 10 respectively. The liquid and plasticity index values are high and its plasticity indices are between 46% and 74%. Free swell index of the clay is between 66% and 175%. Thus the clay layer of BH21 and BH22 is high plastic clay with swelling clay minerals. It is classified as clay of high plastic (CH).

Block M12

At Block M12, exploration was done at two locations as shown in Fig.1b. Borehole 23 (BH23) and borehole 24(BH24) are located diagonally opposite to each other. At BH23 the deposits are soft silty clay followed by silty clayey sand up to 5.5m from the existing ground level followed by weathered rock up to 8.3m, at which depth; the borehole was terminated (Fig 12). The clay layer is in soft condition with minimum and maximum N values of 0 and 3 blows. This layer is classified as clay of high plastic (CH) since liquid and plasticity index values are more than 50% and 43% respectively. The sand layer that follows the clay is classified as clayey sand in which fines are about 22% and sand fractions are more than 60% (Table 11). It is in very dense condition with N value much higher than 100 blows. However there is a decayed wood seam between the depth of 3.15m and 3.45m. Similar organic sandy clay layer is seen at BH22 at depth between 2.6m and 3.4m. The reason for such deposit at these two boreholes is not known, however this formation is problematic deposit and foundation needs to be located below



this deposit. The rock layer that lies below the sand is highly weathered till the depth of 6.3m. However the degree of weathering in rock layer is reduced with depth and core recovery of 8% to 12% is obtained in the rock between the depth of 6.3m and 8.3m.

The deposit encountered at BH24 up to the depth of 2.4m is soft clay as recorded at BH23. But the thickness of residual soil is about 0.4m only in this borehole and weathered rock occurs at depth of 2.75m, which is the highest level of occurrence of rock stratum among the twelve boreholes. The borehole 24 was terminated at the depth of 5.3m, where the deposit was severely jointed rock. The recovery ratios of core samples obtained in this deposit were between 19% and 24%. The clay layer possess same characteristics as that at the clay at BH23 (Table 11) and is classified as CH type clay. The rock layer that lies below the sand is highly weathered till the depth of 6.3m. However the degree of weathering is reduced with depth and core recovery of 19% to 24% is obtained in the rock between the depth of 3.3m and 5.3m.

The overall variation of deposits at locations of each block are combined and presented in Fig 14 to 19 for blocks M7 to M12 respectively. From the figures presented and properties given in tables it is clear that the deposit of the area within the depth of investigation comprises of three layer system. The top layer is clay of high plastic (CH) with liquid limit higher than 60% in general. The swelling quality of the clay is critical to high and is confirmed through the free swell index values more than 60% in most of the samples. Its thickness is found to vary between 1.9m and 2.8m and is in soft condition at most of the locations. The soil of this layer is not even suitable for filling work.

The deposit lies below the clay layer (CH layer) is clayey sand/silty sand. Its thickness is about 3m in general. This layer is in dense condition with recorded N values are close to 50 blows or more except at the transition zone between clay and sand layers. The limitation in this layer is presence of clay lumps, clay patches and organic deposits at certain locations (BH22 & BH23). These lumps are part of highly weathered soil derived from the parent material rock. But the reason for organic deposit is not known. As long as clayey sand layer is intact there may not be change ir their property but due to release in pressure and direct contact with water it will become soft. Thus the condition is not

favorable for isolated footing. Moreover excavation of this layer in presence of water or below the water table will create a problem to locate the foundation in this layer provided the water table is reduced well below so that the soil is not losing its strength and provides good environment for construction. Irrespective of type of foundation, the foundation is to be located below the organic deposit.

The third layer is weathered rock. In this deposit degree of weathering is decreasing with depth and the thickness of strongly weathered portion is around one meter. However the rock stratum at depth below 5.5m is strong deposit however it is, fractured and severely jointed. This rock mass recorded maximum recovery ratio of 31% at BH19 and the RQD is 28%. In general recovery ratio of rock deposit is in the range of 4% to 19% and in most of the locations the RQD is nil. The rock cores obtained from the boreholes are shown in Plate 1 and Plate 2. Rock samples of certain boreholes are tested for strength under unconfined condition and test results are presented in Annexure CS1 & CS2. The unconfined strength of samples is presented below along with secant modulus of samples. The strength of rock of Zone M2 is less than the strength of rock deposit of Zone M1.

S.NO:	Identification	Depth, (m)	Unconfined Strength, (kN/m²)	Secant Modulus (kN/m²)
1	BH19	6.5-7.5	7000	314500
2	BH20	5.8-6.8	16400	324200

The properties of various soil layers both strength and compressibility are obtained from the N values using existing correlations and presented in Table 13. In case of clay Terzaghis' relation is used for obtaining undrained cohesion (C_u) values. The values thus obtained are found to vary between 7.5kN/m² and 15kN/m² in soft clay and the values are in the range between 35kN/m² and 75kN/m² in medium stiff to stiff clay. The strength obtained from UCC test on UDS of BH24 (Annexure U1) is 6.4kN/m², which is in comparison with the value of 7.5kN/m² obtained by empirical correlation. In silty sand/clayey sand angle of shearing resistance (Φ) is obtained using Meyerhof recommendations. However the modification suggested by Houch for the percentage



fines present in the deposit is applied. The ϕ values obtained are varying between 32° and 42°.

In sand compressibility parameter is obtained by the relation C=1.9 q_c/σ'_0 , where q_c -cone resistance and σ'_0 -effective overburden pressure. This procedure was developed by DeBeer and Martens (1957) and later on modified by Meyerhof to determine the elastic settlement in non plastic cohesionless deposit. IS 8009 (Part I), is also recommends this method to obtain immediate settlement. In the absence of cone resistance (q_c), it is considered equal to 220N to 300N (kN/m²) since the deposit is SP/SM type. The strength and compressibility parameters thus obtained are summarized in Table 13.

In the absence of consolidation test results, the compressibility parameter, m_v (=1/E) of clay deposit of Zone M2 is obtained from the chart of Stroud (1975) which accounts for the plasticity of clay fines and the value is based on N_{60} value and is equal to 1/F N_{60} (m^2/kN). The "F" is varying between 420 and 480 in medium to stiff clays. The shear strength of rock is obtained from the UCC test conducted on core samples of BH19 and BH20 and the values are $7000kN/m^2$ and $16400kN/m^2$ respectively. The C_u values are also obtained for highly weathered rock based on Cole and Stroud (1977) chart and the values thus obtained are presented in Table 13.

7. Ground water quality

The ground water table at all the boreholes is monitored and the levels are reported in section 5. Water samples are collected and tested for pH, sulphates and chlorides. Since the water is brackish, it is also decided to test the soil for above properties. The chemical test results are presented below:

Chemical test results of water and soil samples

Location	Sam ple	Depth m	pН	Sulphate (SO ₄) ppm	Chloride ppm	Remarks
Block M7	viotos.	1.5 (BH13)	7.65	745	15575	Sulphates and chlorides
Block M9	water	1.5 (BH18)	8.1	875	13450	are very high
Block M7	soil	1.5(BH14)	8.1	350	750	Sulphates and chlorides
BIOOK IVI		1.5(1511111)	0,1	330		are high



In water samples tested, pH is close to neutral, but chlorides and sulphates are very high and the amount of chlorides present in ground water indicates that the ground water of this area is just like sea water.

In soil, the contents of sulphates and chlorides are more in top clay layer. The results of tests on soil and water are to be reconfirmed. Sulphates and chlorides both in soil and water are more than the permissible limits as per IS 456 (Refer Table 4). Since ground water is very poor in quality suitable measure is to be taken to protect concrete and rebars from sulphate attack and corrosion of reinforcement. The clayey soil is not only plastic but also contains chlorides and sulphates in high quantity, hence not suitable for filling.

8. Summary

- 1. The top soil is highly plastic clay at all the borehole locations. Its thickness is found to vary between 1.9m and 2.8 m. It is susceptible for volume change due to seasonal variation in the moisture content. Free swell index value is as high as 100% at a few locations indicating clay is active. It is in medium stiff to stiff condition at Block M7 and M8 and rest of the locations the clay is in soft state. Native clay soil is not at all suitable for any construction work including back fill of basement and foundations.
- 2. The deposit below the depth of 2.5m from the existing ground level is residual deposit (highly weathered rock), which is a strong layer. The minimum N value recorded in this layer is 24 blows, which indicates that the deposit is in medium dense state. Further fines are less than 25% in sand at most of the location except at the transition zone between clay and sand and the balance content is dominantly sand and gravel fractions. This layer is strong enough to support any shallow foundation. However presence of clay lumps and clay patches need to be considered while deciding the foundation type. However at two locations sand is



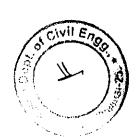
mixed with organic soil, but this layer is at shallow depth; hence foundation can be located below this layer.

- 3. The deposit below 5m is highly fractured rock which has recorded refusal N value. The recovery ratio of rock samples found to vary between 0 and 19% at most of the depths of rock deposit, which indicates that the rock is jointed and fractured. However a value of 31% is also recorded at certain depth of rock deposit. RQD is generally zero and more than 25% is recorded in rock samples obtained at depth below 6m at two boreholes located on the south western side of Zone M2. The maximum RQD is 28%, which is recorded in BH19 at the depth between 6.5m and 7.5m.
- 4. The water table level is at shallow depth (1m to 1.4m) from the existing ground level. The lowest level of ground water table at M2 area is +0.009m (RL) during the time of investigation (March 2013). The sulphates and chlorides are present in both soil and water samples.

From the summary presented it is evident that the deposit of area is suitable for providing foundation at shallow depth. However the top soil to a depth of 2.5 to 3.0m is poor, hence foundation cannot be located in this layer. Therefore it is felt essential to locate the foundation at a minimum depth of 3.2 from the existing ground level. The depth suitable to locate the foundation is 3.2m or below from the existing ground level. The maximum variation in the reduced level of borehole locations is 0.5m (maximum + 1.688m and minimum +1.200m); hence minimum level of foundation shall be -2.0m (RL). However depth of foundation for each block of Zone M2 area is given in the Section 10.

9. Selection of foundation

The subsurface condition of deposit of area is very much suitable for shallow foundation except that the foundation needs to be taken below the top clay layer. In this case it is suggested to locate the foundation at a minimum depth of 3.2m from the



existing ground level. In order to decide the depth of foundation of the blocks, N value more than 50 blows and location of water table are compared as below:

			-F						
		RL of	WT RL,	Remarks					
No:			(m)						
M7	-1.462	-1.512	+0.288m	Water table is above the					
		,		foundation level					
M7	-1.735	-1.785	+0.015m	Water table is above the					
				foundation level					
M8	-1.061	-1.061	+0.039m	Water table is above the					
				foundation level					
M8	-1.910	-1.910	+0.140m	Water table is above the					
				foundation level					
M9	-1.658	-1.658	+0.092m	Water table is above the					
				foundation level					
M9	-1.741	-1.741	+0.009m	Water table is above the					
				foundation level					
M10	-2.491	-1.891	+0.109m	Water table is above the					
				foundation level					
M10	-1.900	-1.900	+0.150m	Water table is above the					
				foundation level					
M11	-2.396	-1.946	+0.154m	Water table is above the					
				foundation level					
M11	-3.233	-2.733	+0.267m	Water table is above the					
				foundation level					
M12	-2.550	-2.550	+0.200m	Water table is above the					
				foundation level					
M12	-1.505	-1.505	+0.295m	Water table is above the					
				foundation level					
	M12	No: stratum at N>50, (m) M7 -1.462 M7 -1.735 M8 -1.061 M8 -1.910 M9 -1.658 M9 -1.741 M10 -2.491 M11 -2.396 M11 -3.233 M12 -2.550	No: stratum at N>50, (m) min.Depth of foundation, (m) M7 -1.462 -1.512 M7 -1.735 -1.785 M8 -1.061 -1.061 M8 -1.910 -1.910 M9 -1.658 -1.658 M9 -1.741 -1.741 M10 -2.491 -1.891 M10 -1.900 -1.900 M11 -2.396 -1.946 M11 -3.233 -2.733 M12 -2.550 -2.550	No: stratum at N>50, (m) min.Depth of foundation, (m) (m) M7 -1.462 -1.512 +0.288m M7 -1.735 -1.785 +0.015m M8 -1.061 -1.061 +0.039m M8 -1.910 -1.910 +0.140m M9 -1.658 -1.658 +0.092m M9 -1.741 -1.741 +0.009m M10 -2.491 -1.891 +0.109m M10 -1.900 +0.150m M11 -2.396 -1.946 +0.154m M11 -3.233 -2.733 +0.267m M12 -2.550 -2.550 +0.200m					

From the comparison made it is clear that foundations are to be located below the water table. The water table level reported is obtained from the borehole during investigation; there is a possibility for variation in the water table level. Therefore it is suggested to ascertain the water table level at each block at least at two corners before proceeding with the work of foundation. Normally the actual water level may be higher than recorded in the boreholes. It is suggested to locate the foundation a few centimeters above the water level in order to avoid excavation below the water table otherwise excavation below water table makes the soil to lose its strength. However at Zone M2



area the foundations are to be located below the water table, hence dewatering is essential.

The bearing capacity and settlement of foundation for the minimum depth of foundation given in the table are determined. The bearing capacity is determined for the raft foundation of size 23mx46m (approximate) using Teng (1961) equation and bearing capacity equation given in IS6403. The allowable bearing pressure is obtained for 25mm settlement using Teng equation and it varies between 358kN/m² and 403kN/m² for the N values between 41 and 46 respectively. The net safe bearing capacity value obtained from IS6403 for $\phi=36^{\circ}$ is $1300kN/m^2$ for FS=3. The soil at the foundation level of certain boreholes is stiff sandy clay with fines around 25%. Though thickness of sandy clay layer is less the bearing capacity value is determined by considering the lowest N value of 41 is 358kN/m² for a settlement of 25mm. Thus it is sure that the soils at the foundation levels are having good bearing strength and more over raft foundation of large size will provide higher bearing resistance and the settlement is real concern. recommended bearing capacity is 250kN/m². The bearing capacity is reduced from the minimum value of 358kN/m² obtained, in order to account for the undesirable condition like presence of clay pockets. The average load intensity expected at the foundation level for the combination of load may not exceed 220kN/m2, which is close to the bearing capacity recommended. The shallow foundation like isolated footing is not considered because of heterogeneous nature of soil (week zones like clay patches and clay lumps). However as an academic exercise the capacity was worked for the isolated footing of 2.5mx2.5m for the $\phi'=36^{\circ}$. The net safe bearing capacity obtained is 190kN/m^2 , which is less than the expected average pressure of 220kN/m² of raft foundation. However the contact pressure expected will be more than 190kN/m² if isolated footing is proposed to adopt for each column. If the bearing capacity is limited to 190kN/m² then foundations of columns are to be combined. Thus only option to support the buildings of stilt+eight storeyed buildings in the Zone 'M2' of Perumbakkam project is raft foundation.

The settlement of raft foundation is also worked out for the soil conditions of individual borehole for the net pressure of 250kN/m². The foundation is supported in

silty sand / clayey sand layer which is non-plastic with course fractions around 70% followed by weathered/fractured rock. Therefore elastic settlement of foundation is obtained using DeBeer and Martens (1957) equation. The elastic settlement obtained at various locations is less than 25mm for the contact pressure of 250kN/m². Thus the raft foundation is the ideal choice for supporting the foundations of proposed stilt + eight storeyed blocks M7 to M12 at Zone 'M2'.

The one more issue is depth of foundation of each block can be different because of variation in depth of occurrence of bearing stratum within the Zone M2. Further providing uniform depth of foundation for all the six blocks (M7 to M12) will lead to more excavation at locations of certain blocks. The minimum depth of foundation (RL) at various blocks is varying between -1.75m and -2.75m. In this area the water table level at boreholes is found to vary between +0.51m and +0.009m, and is above the recommended level of foundation, hence interference of water table cannot be avoided while executing the earthwork excavation to reach proposed level of foundation. The foundation excavation in presence of water is to be avoided. Adopt suitable dewatering method to lower the level of water table at least to a level of 0.5m below the foundation level.

10. Recommendations

The subsurface exploration conducted at Zone 'M2' confirms presence of good bearing stratum at a depth of 3.2m at Block M7 and at a depth of 4m at block M11. Thus occurrence of good bearing stratum is at shallow depth on the western side of Zone M2 and slopping towards east direction. However the deposit at the depth below 5.5m is certainly weathered rock over entire area of Zone M2. The top layer is soft at most of the locations and at locations wherever clay is medium stiff to stiff possesses volume change characteristics. This layer will exhibit high swelling (DFS>100%). Thus it is recommended to locate the foundation at a minimum depth of 3.2m from the lowest ground level. For the structure of stilt + 8 storeyed building it is recommended to support the structure on a raft foundation. The recommended bearing capacity of soil for the raft foundation of 23m x 46m (approximate size) is 250kN/m². Though the soil below the



depth of foundation possesses higher bearing strength, it is advised not to exceed the value of 250kN/m² because of non-homogenous nature of the deposit. Recommended level of foundation for the blocks M7 to M12 is as below:

Sl.No:	Block	Reduced level of Foundation,(m)
1	M7	-2.0
2	M8	-2.0
3	M9	-2.0
4	M10	-2.0
5	M11	-2.75
6	M12	-2.6

The level of foundation refers to base of a raft and the raft shall be laid on leveling course followed by sand cushion of adequate thickness each as per the practice in the board.

11. Precautions

- 1. The top soil to the depth of 3.0m is poor and highly swelling (expansive) hence does not suitable for any construction or filling work.
- 2. The maximum depth of occurrence of water table in zone M2 is +0.009m (RL) and the soil at this depth is clayey at most of the location hence excavation under this condition without dewatering will lead to collapse of cut and also reduction in strength of soil because of seepage through the bearing stratum.
- 3. Earth work excavation particularly below the water table to be allowed unless the water level is lowered to minimum depth of 0.5m from the recommended level of foundation. Adopt suitable scientific method for dewatering.
- 4. The depth of foundation recommended for each block is minimum depth of foundation. There may be chances for variation in foundation depth because of uncertainty in the characteristics of highly weathered residual deposit in the Zone M2 area. Improper dewatering and submergence of weathered soil may lead to significant reduction in strength, which may demand foundation at deeper depth than recommended to realize bearing capacity of 250kN/m². Do not reduce the foundation



- depth without obtaining proper approval from the consultant in case of good bearing stratum is met at higher level than the recommended level of foundation.
- 5. The water table in this area is at shallow depth. The seepage of water at the interface of weathered rock and soil cover will be critical hence conduct a pilot study to determine seepage parameters of deposits and to design suitable dewatering system. Technical support required for designing the dewatering system will be provided if required by the client. No case seepage is permitted directly through the foundation soil i.e. seepage of water shall be away from the excavation area (i.e. foundation area) and not towards the excavation area.
- 6. The quality of ground water is not suitable for any construction work especially for foundation construction. Since the environment of both ground water and soil is aggressive, this will lead to sulphate attack on concrete and corrosion of reinforcement. The concrete and steel need to be protected from the aggressive action. Thus provide minimum cover of 75mm in addition to any other protective measures considered suitable. Obtain opinion from structural engineer for protecting foundation elements and part of columns and beams buried below the ground. Further the cement quality and the content shall satisfy the requirement of Table 4 of IS 456-2000.
- 7. Since the ground water is not satisfying the requirement, use good water for all concrete related work. Minimum grade of concrete recommended for the foundation work is M25. Follow the conditions relevant to quality of water for concrete work as per IS 456-2000 including minimum cover thickness.
- 8. For filling works both inside the basement and outside around the building use good earth. The native soil particularly the high plastic clay is not at all suitable for any construction work including basement filling.
- 9. The basement filling will be more than 3.0m hence conventional flooring for the ground storey may lead to settlement problem on later days. It is suggested to provide RCC floor for ground floor base slab.



10. In case of any variation observed from the soil profile reported while execution of foundation work, bring it to the notice of consultant immediately for suitable advice. Do not change the recommended level of foundation without the knowledge of foundation consultant.

Dr. K. ILAMPARUTHI

Project Co-Coordinator & Professor and Chairman Department of Civil Engineering Anna University Chennai – 600 025

Dr. K. ILAMPARUTHI, M.E.,Ph.D., Professor & Chairman Faculty of Civil Engineering Anna University, Chennal-600 025,

Figure A1 Perumbakkam Project – Zones of Investigation

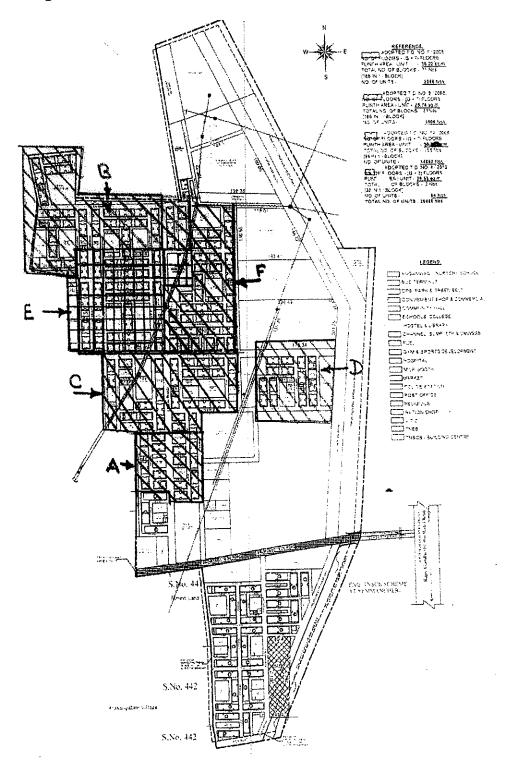
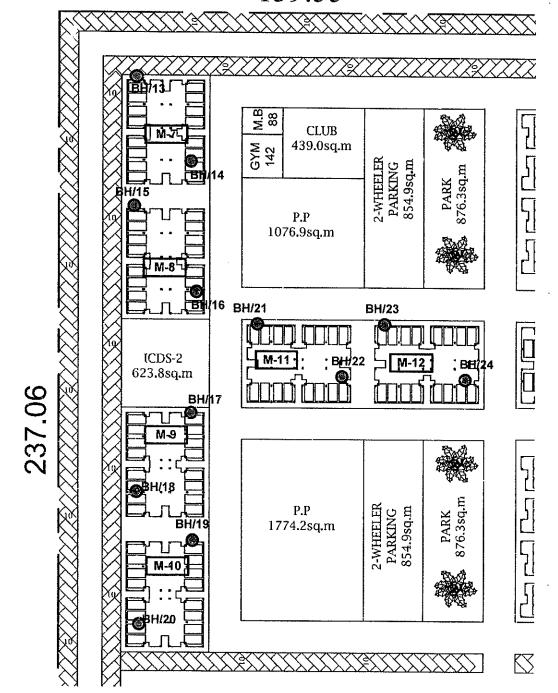




FIGURE 1B LOCATION OF BORE HOLES (ZONE M2)

SOIL INVESTIGATION FOR THE PROPOSED MIG BLOCKS TNSCB, PERUMBAKKAM

139.55



Boreholes are located 5.0m from the boundary on either side.

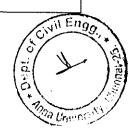


FIGURE 2 SOIL PROFILE AND SPT N VALUES AT BH 13 - M2

PROJECT NO: SF/KI-48/Zone M2/PMPKM BORE HOLE NO: BH/13

The Univer

Project

MIG Tenements, TNSCB, Chennai

Site

Perumbakkam, M2 Zone

Co-ordinates

: Block M7

Diameter and type of boring : 150mm Rotary boring with drilling mud circulation

10-Mar-2013 Date of start 11-Mar-2013 Date of finish 1.40m

GWL from GL Ground level RL 1.688m

Ę	<u>e</u>		Dep				SPT	VST			
Depth from GL(m)	Soil Profile	Field Description	sam colle	,	Test		SPT	blow	cour	nts	RD /
g 4	扊	·	UDS	DŞ	depth m	15	30	45	60	N**	Consistency
-			000	0.50		13	30	40	00	-14	
		Yellowish grey silty clay with few stones		0.50		ŀ					Medium stiff
1.0				0.75	0.75	2	4	6	11	10	
1.9		Greyish brown sandy silty clay with stones	1	1.50	1.50	5	8	17	23	25	Stiff
2.0					1.55	Ĭ					
		Greyish brown clayey silty fine to coarse sand with sandy clay lumps		2.25	2.25	10	15	32		47	Dense
3,0		sandy day lumps		3.00	3.00	38	50/8	cm		>100	
	, "					50"				ا	
4.0	* • •	Greyish brown dirty fine to coarse sand with		3.75	3.75	50/8	scm			>100	
	"	weathered stones (weathered disintegrated rock)		4.50	4.50	30/4	4cm			>100	Very dense
5.0	*					<u>. </u>			1		
5.5				<u> </u>	5.50 TC con					RB	
6.0		Yellowish grey highly weathered fractured rock	5.50-6.3	30	6.30			d		RB	Very weak
6,3	戵		l		Diamor				IX siz		
7.0		Brownish grey highly / completely weathered	6.30-7.3	30	recove						Weak
		severely jointed rock			Diamor	nd co	re dri	lina t	JX siz	e.	''''
8.0			7.30-8.3	30	recove					,	1841
-	譁	Br grey highly weathered severely jointed rock	 		 						Weak
9.0	1										i l
	1			1							
10.0	1										
11.0	4										
	1										
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	1										
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16.0	4						1				
17.0	녈				1						
	1										
18.0)							ŀ			
19.0	2										
	1	TC core drilling from 5.50m to 6.30m									
20.6)	DC core drilling from 6.30m to 8.30m									·
	1_				<u> </u>						L KE
		rehole terminated at 8.30m ote: SPT Conducted using winch cat-head device, N values re	norted a	re close	to N						(6)\\
L	1 14	ote. or i conducted using winth cat-head device, it values re	Ported at	14 CIUSE	W 1470						-/3/ \

FIGURE 3 SOIL PROFILE AND SPT N VALUES AT BH 14 - M2

PROJECT NO: SF/KI-48/Zone M2/PMPKM BH/14 BORE HOLE NO:

Project

MIG Tenements, TNSCB, Chennai

Site

Perumbakka n, M2 Zone

Co-ordinates

: Block M7

Diameter and type of boring ; 150mm Rotary boring with drilling mud circulation

Date of start Date of finish GWL from GL

12-Mar-2013 13-Mar-2013

1.40m 1.451m Ground level RL

										······	
Ε <u>Ξ</u>	흹	!					SPT	/ VST	·		pn/
Depth from GL(m)	Soil Profile	Field Description					SPT	blow	coun	ıts	
g (y	Soil					15	30	45	60	N**	
]		Vellowish grey silty clay with roots in the top 0.40m		0.00							Medium stiff
1.0		tologion and only only man roots in the top of the	UDS DS m 15 30 45 60 N 0.50 0.50 0.75 2 2 3 4 0.50 0.75 0.75 2 2 3 4 0.50 0.75 0.75 2 2 3 4 0.50 0.50 0.75 0.75 2 2 3 4 0.50 0.50 0.75 0.75 2 2 3 4 0.50 0.50 0.75 0.75 2 2 3 4 0.50 0.50 0.50 0.75 0.75 2 2 3 4 0.50 0.50 0.50 0.50 0.75 0.75 2 2 3 4 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.	5							
1.4				4 50	4 50	١,	,	40	4.2	47	
2.0		Yellowish grey silty clay with white stones and gravel		1.50	1.50	4	′	10	13	17	Stiff
2.2		Greyish brown clayey silty sand with sandy clay		2 25	2 25	Я	12	13	16	25	Madium dansa
3.0		lumps & weathered stones		2.20	Į				.		Widolulli delise
		Greyish brown dirty fine to coarse sand with		3.00	3.00	21	32	50		82	Vary dones
4.0		weathered stones		3.75	3.75	32	50/	12cm	ì	>100	very dense
		Brownich grow dirty fine to coarse sand with	1]	l	l	l	l	1	>100	
	1/2	weathered stones		4.50				ч		RB	Very dense
5.0	**		 	L				<u> </u>		1,5	
5,7		Greyish brown highly weathered fractured rock	5.00-5.1	70	5.70	Ret	oun	d			Very weak
6.0				70	Diamor	nd co	re dri	lling 1	√X siz	:e,	
			15.70-6.7	70	recover	y 15	% RC	D nil			
7.0	Ħ	Greyish brown highly weathered severely jointed			Diamor	ad co	re dri	llina I	JX siz	7A	Weak
		rock	6.70-7.7	70					.,,	,	Medium stiff Stifl Medium dense Very dense Very dense Very dense Very weak
8.0			 		 				1007.		1
8.2		Describe and high weathered stooks inited rook	7.70-8.1	70						ze,	
1		(Granitic gneiss)	<u> </u>	1	1.00010	1	10, 11	T	·· T	T -	Moderate
9.0	1	(Granitic grieiss)									
	1							İ			
10.0	-										
	1						ĺ				
11.0	1							Ì			
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14.0	4				1			1			
	1										
15.0	1									1	
16.0)			1	1						
	7	-									1
17.0	,										
1	1										
1										[
18.0	4										
	1										
19.0	그			1							
		TC core drilling from 5.00m to 5.70m									
20.0	0	DC core drilling from 5.70m to 8.70m									
	_				<u> </u>				<u></u>		
		rehole terminated at 8.70m			4 A.F						/
	**N	ote: SPT Conducted using winch cat-head device, N values re	ported a	re close	10 N ₇₀						15/ 1

FIGURE 4 SOIL PROFILE AND SPT N VALUES AT BH 15 - M2

PROJECT NO: SF/KI-48/Zone M2/PMPKM BORE HOLE NO: BH/15

Date of start

13-Mar-2013

MIG Tenements, TNSCB, Chennai Perumbakkam, M2 Zone

14-Mar-2013 Date of finish

Co-ordinates

Project

Site

: Block M8

Diameter and type or horing : 150mm Rotary boring with drilling mud circulation

1.30n. GWL from GL 1.339m Ground level RL

GL(m) Soil Profile		Dept sam		Tark	;	SPT	/ VST	-		RD/	
GL(m) Soil Profile	Field Description	colle		Test depth		SPT	blow	coul	nts	Consistency	
S S		UDS	DS	m	15	30	45	60	N**		
0.5	Brownish grey silty clay with roots		0.50	,						Medium stiff	
1.7	Yellowish grey silty clay		0.75			3	5	7	8	Medium stiff	
2.3	Greyish brown clayey silty sand with weathered stones		1.50			9	12	17	21 84	Med dense	
3.0	Yellowish grey dirty fine to coarse sand with sandy clay lumps		2.25 3.00	ļ	l	Į .	I		>100	Very dense	
"'∭		3.00-3.6	i0m	3.60	Reb	oun	d		RB	,	
1.0	Brownish grey highly weathered fractured rock	3.60-4.6	60	Diamor recove		re drii	lling N	4X sia	ze, 	Weak	
5.0 5.6		4,60-5.6	30	Diamor recove		re dri	lling M	√X si:	ze,		
6.0 6.0	Brownish grey completely weathered severely jointed rock	5.60-6.6	30	Diamor recove			lling t	√X si	ze,	Weak	
7.0	Greyish partly weathered jointed rock (granitic gneiss)	6.60-7.6	50	Diamoi recove					ze,	Moderate	
9.0											
5.0											
7.0	,			.,							
8.0											
20.0	TC core drilling from 3.00m to 3.60m DC core drilling from 3.60m to 7.60m									Eng.	
В	prehole terminated at 7.60m		1						/	<u> </u>	
	orehole terminated at 7.60m Note: SPT Conducted using winch cat-head device, N values re	eported a	re close	to N ₇₀					$-\frac{1}{1}$	\overline{U}	

FIGURE 5 SOIL PROFILE AND SPT N VALUES AT BH 16 - M2

PROJECT NO: SF/KI-48/Zone M2/PMPKM BORE HOLE NO: BH/16 14-Mar-2013 Date of start

Project Site

MIG Tenements, TNSCB, Chennai

Perumbakkam, 1/12 Zone

Co-ordinates

; Block M8

Diameter and type of boring ; +50mm Rotary boring with drilling mud circulation

15-Mar-2013 Date of finish GWL from GL 1.10m 1.240m Ground level RL

		***							•		
П	<u>ē</u>		Dept	th of							
GL(m)	Soil Profile	Field Description	sam		Test		SPT	RD/			
-ত	ğ		colle		depth	SPT blow cour					Consistency
	S	Mallandah ann alle alau (da)	UDS	DS	m	15	30	45	60	N**	
0.5		Yellowish grey silty clay (dry)		0.50							
1.0				0.75	0.75	2	4	6	7	10	Medium stiff to
1		Yellowish grey and brown silty clay with few stones		4.50	4.50	_		40	امدا	4.0	stiff
.0				1.50	1.50	7	9	10	14	19	
2.1	▓▋	Yellowish grey clayey silty sand with sandy clay		2.25	2.25	10	14	27	32	41	Dense
.0]	%	lumps				ł					
3,8		Brownish grey dirty fine to medium sand with sandy		3.00	3.00	28	32	50		82	
.0		Crayleb distribute to page and with weathered	-	3.75	3.75	50/1	3cm			>100	Very dense
4.7	,	Greylsh dirty fine to coarse sand with weathered stones (wdr)			4.50	Reb	ounc	į		RB	
.0		otorico (var)			TC core	a drill	ina				
_		Brownish grey highly weathered fractured rock	4.50-5.8	30			-		Very weak		
i.8 .0			ļ		5.80	Ret	ounc	RB			
1			5.80-6.8	30	Diamor		e.				
.0		Yellowish grey highly / completely weathered			recover	y 10°	%, RC		<u> </u>		
~		calcareous sandstone	6,80-7,8	30	Diamor			ze,	Weak		
.0					recove			D ni	1		<u> </u>
9.1			7.80-8.3	8.30	DC Co 8.30	e dri	ling 13cm	>100			
	8	Brownish grey dirty fine to coarse sand with weathered stones	9 20 0		TC cor			1	Very dense		
.0 9.2	111	weathered stones	0.30-9.	8.30-9.20		e ami	iriy			<u> </u>	
		Greyish partly weathered and severely jointed rock	9.20-10.20		Diamor			ze,	Weak		
.0		, , , , , , , , , , , , , , , , , , ,		,	recove	ry 16'		_			
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3.0											
1,0											4
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0.0											
į											
0.6											d types
											1
0.								}			
8.0											
0.0											
-	1	TC core drilling from 4.50m to 5.80m									
0.0	1	DC core drilling from 5.80m to 8.30m & 9.2m to 10.20m									
	1				-						111
	Bor	ehole terminated at 10.20m									1./
	1**Nr	ote: SPT Conducted using winch cat-head device, N values re	ported ar	e close	to N ₇₀						15/

FIGURE 6 SOIL PROFILE AND SPT N VALUES AT BH 17 - M2

PROJECT NO: SF/KI-48/Zone M2/PMPKM BH/17 **BORE HOLE NO:** 16-Mar-2013 Date of start 17-Mar-2013 Date of finish 1.40m GWL from GL

Ground level RL

1.492m

Project

MIG Tenements, TNSCB, Chennai

Site

Perumbakkam, M2 Zone

Co-ordinates

: Block M9

Diameter and type of biging : 150mm Rotary boring with drilling mud circulation

SPT / VST Depth of Depth from GL(m) RD / samples Test SPT blow counts Field Description collected Consistency depth Soil UDS 15 30 45 60 DS m Medium stiff Brownish grey silty clay with sand 0.50 0.5 Very soft 1.0 0 0.75 Brownish grey soft silty clay 0.75 Sunk @ SPT wt 0 Dark grey soft silty clay with gravel and organic 1.50 1.50 Very soft 2.0 material 2.3 23 29 38 7 15 2.25 2.25 Greyish clayey silty fine to coarse sand with Dense 3.0 weathered stones 3.00 9 17 24 33 41 3.00 Brownish grey clayey silty fine to coarse sand with 3.75 50/09cm 3.75 >100 Very dense weathered stones 4.00 Rebound RB TC core drilling 4.00-5.00 5.00 Rebound RB Dark greenish grey completely weathered fractured 5.0 Very weak TC core drilling 5.00-6.00 6.00 Rebound RB 6.0 Diamond core drilling NX size Yellowish grey highly weathered severely jointed Weak 6.00-7.00 recovery nil rock 7.0 Diamond core drilling NX size Brownish and light yellowish fully weathered severely 7.00-8.00 recovery 9%, RQD nil Weak jointed rock 8.03 Diamond core drilling NX size 8.00-9.00 Weak to Yellowish grey and grey highly weathered severely recovery 16%, RQD nil moderate 9.0 jointed rock 10.0 11.0 12.0 13.0 14.0 15.0 16.0 17.0 18.0 19.0 TC core drilling from 4.00m to 6.00m DC core drilling from 6.00m to 9.00m 20.0 Borehole terminated at 9.00m

33

**Note: SPT Conducted using winch cat-head device, N values reported are close to N₇₀

FIGURE 7 S OIL PROFILE AND SPT N VALUES AT BH 18 - M2

PROJECT NO: SF/KI-48/Zone M2/PMPKM BORE HOLE NO: BH/18

Project

MIG Tenements, TNSCB, Chennai

Site

Perumbakkam, M2 Zone

Co-ordinates

: Block M9

Diameter and type of boring : 50mm Rotary boring with drilling mud circulation

Date of start Date of finish

18-Mar-2013 19-Mar-2013

1.40m GWL from GL 1.409m Ground level RL

=	ø		Dept	h of		;					
CE(π)	Soil Profile	Field Description	sam colle		Test depth		SPT		coun		RD / Consistency
5	တိ		UDS	DS	m	15	30	45	60	N**	
		Yellowish grey silty clay with black patches		0.50			!				Medium stiff
1.0		Brownish grey silty clay with reddish brown patches		0.75	0.75	1	1	1	2	2	Soft
2.0		Yellowish grey and brownish silty clay		1.50	1.50	2	3	5	11	8	Medium stif"
2.9 3.0		Brownish clayey silty fine to medium sand / sandy silty clay		2.25	2.25	6	10	14	18	24	Med dense
3.7	7,	Greyish brown dirty fine to coarse sand with weathered stones		3.00	l	ł	ł	Ì		74	Very dense
4.0		Yell grey clayey silty fine to coarse sand with		3.75	3.75 4.50		ļ	1	ŀ	>100 RB	Very dense
4.5 5.0		weathered stones (wdr) Yellowish grey highly / completely weathered	4 50 5 1	<u> </u>	TC cor					'``	Very weak
5.5		fractured rock	4.50-5.		5.50			RB	10,,		
6.0		Greyish brown & grey completely weathered severely jointed rock	5,50-6.	50	Diamoi recove			lling l	VX si	ze	Weak
6.5 7.0		Brownish and grey highly weathered severely jointed	6.50-7.	50	Diamond core drilling NX size recovery 15%, RQD nil						Weak
8.0		rock	7.50-8.	50	Diamond core drilling NX siz recovery 22%, RQD nil					ze	VVCul
9.0											1
10.0	14										
11.0	2										
12.0	2										
13.0	2										
14.	0										
15.	0										
16.	0										
17.	0										
18.	0										
19											
20		TC core drilling from4.50m to 5.50m DC core drilling from 5.50m to 8.50m									
	L				l					l	مصنب (۱۹۲۶) میرنامس
	В	orehole terminated at 8.50m		oro oloca	to M						- (N.E.)
	1	Note: SPT Conducted using winch cat-head device, N values n	еропеа	are close	; (U N70						/3/ 、

FIGURE 8 SOIL PROFILE AND SPT N VALUES AT BH 19 - M2

PROJECT NO: SF/KI-48/Zone M2/PMPKM BORE HOLE NO: BH/19

Project

MIG Tenements, TNSCB, Chennai

Site

Perumbakkam, M2 Zone

Co-ordinates

; Block M10

19-Маг-2013 Date of start Date of finish

GWL from GL

20-Mar-2013 1.30m 1.409m

GL(m) Soil Profile		Depi sam		Т	ļ	SPT		RD/			
GL(m) Soil Profile	Field Description	collected		Test depth	SPT blow cour				ıts	Jonsistency	
ŏ		UDS	DS	m	15	30	45	60	N**		
0.6	Br grey silty clay with brown & black patches		0.50							Medium stiff	
.0 1.4	Yellowish grey soft silty clay with reddish brown patches		0.75	0.75	0	1	1	1	2	Soft	
2.4	Greyish soft silty clay with reddish brown patches		1.50			SPT		1	0	Very soft	
.0	Brownish grey dirty fine to coarse sand weathered		2.25 3.00			12 20	19 24	27 31	31 44	Dense	
1.0	stones		3.75		l]		>100	1	
	MANUAL CONTRACTOR CONT		0.70	4.50		l) d	1	RB		
5.0	Brownish grey completely weathered / highly weathered fractured rock	4.50-5.5		TC core						Very weak	
5.5	Woulder Hadiated Fook	4.50-5.5	10	5.50	Reb	ounc	1		RB		
6.7	Brownish highly weathered severely jointed rock (siltstone)	5.50-6.5	50	Diamon recover					e,	Weak	
7.0	Light brownish and light grey widely jointed hard rock (siltstone)	6.50-7.5	50	Diamon recover					:e,	Strong	
.0											
0.01											
0.0											
1.0										,	
2.0											
1.0											
1.0											
5.0											
3.0											
7.0	. •										
3.0											
					Ì						
9.0	TC core drilling from 4.50m to 5.50m										
1	DC core drilling from 5.50m to 5.50m	1									
0.0	_				1		1	1		180	

FIGURE 9 SCIL PROFILE AND SPT N VALUES AT BH 20 - M2

PROJECT NO: SF/KI-48/Zone M2/PMPKM BORE HOLE NO: 20-Mar-2013 Date of start

Project

MIG Tenements, TNSCB, Chennai

Site

Perumbakkam, M? Zone

Co-ordinates

: Block M10

Date of finish GWL from GL

1.10m 1.250m

21-Mar-2013

ile		Depth of				SPT					
Soil Profile	Field Description	sam colle		Test depth		SPT blow cour			nts	RD / Consistency	
S		UDS	DS	m	15	30	45	60	N**	-	
	Yellowish grey silty clay		0.50							Soft	
	Light grey very soft silty clay with reddish brown patches		0.75	0.75	Su	l nk@ i	SPT	wt	0	Very soft	
	Brownish grey silty clay with gravel and sand		1.50			4	6	8	10	Medium stiff	
	Yellowish grey clayey silty fine to coarse sand with weathered stones		2.25 3.00	•				,	24 >100	Very dense	
	Vallancial			3.75 Rebound					RB		
	Yellowish grey completely / highly weathered fractured rock	3.75-4.8	0	TC core						Very weak	
				4.80	Ret	oun	<u></u>		RB		
	Light brownish grey weathered closely jointed rock	4.80-5.8			Diamond core drilling NX size, recovery 12%, RQD nil				e,	Weak to moderate	
	Light brown and grey widely jointed hard rock (siltstone)	5,80-6,8	10	Diamon recover					£8,	Hard	
	TC core drilling from 3.75m to 4.80m										
	DC core drilling from 4.80m to 6.80m	<u></u>								11000.	
	hole terminated at 6.80m	norted a-	o doco i	la N						3 / \	
I MO	te: SPT Conducted using winch cat-head device, N values re	ported an	e ciuse l	U 1170						<u>5</u> 5√	

FIGURE 10 SOIL PROFILE AND SPT N VALUES AT BH 21 - M2

PROJECT NO: SF/KI-48/Zone M2/PMPKM BORE HOLE NO: BH/21

Project

MIG Tenements, TNSCB, Chennai

Site

Perumbakkam, M2 Zone

Co-ordinates

: Block M11

Diameter and type of boring : 150mm Rotary boring with drilling mud circulation

22-Mar-2013 Date of start 23-Mar-2013 Date of finish GWL from GL 1.20m Ground level RL 1.354m

_		a type of coming . To other troating to the state of the									
GL(m)	elle Elle		Depl			· · · · · ·	SPT/	VST	•		DD 1
틧.	Soil Profile	Field Description	sam colle		Test depth		SPT	blow	cour	nts	RD / Consistency
၅	Soil		UDS	DS	m	15	30	45	60	N**	O MOIOCONO,
1.6		Yellowish grey medium stiff silty clay		0.50							Medium
<u>0</u>		Yellowish grey soft silty clay with yellow patches		0.75	0.75	1	1	1	2	2	Soft
.9 0		Lt grey soft silty clay with reddish brown patches		1.50	1.50	1	3	4	10	7	Soft
.3		Yell brown and grey sandy silty clay with gravel									Medium stil
.0		Yell grey clayey silty sand with sandy clay lumps and weathered stones		2.25 3.00	2.25 3.00			31	30	44 49	Dense
.0		Would do not		3.75	3.75	23	50/1	2cm	l ì	>100	
寸	1	Yellowish grey dirty fine to coarse sand			4.50	1	1 1		1	RB	Very dense
1.5 .0		Yellowish grey highly weathered fractured rock	4.50-5.5	50	TC core	e drill	ing				Very weak
5.5					5.50					RB	
.0			5,50-6.5	50	Diamor recover					.e.	
.0		Greyish weathered severely jointed rock	6.50-7.5	50	Diamor recover					£6,	Weak
3.0			7,50-8.5	50	Diamor					ze,	
8.1		Brownish & grey weathered closely jointed rock			recove	ry 18	%, KU	וט טו	1	т——	Moderate
9.0											
1		·			İ						
0.0											
1		·						-			
1.0											
1											
2.0											
3.0										ļ	
	1										
1.0											
5.0]						
3.0											
:									:		[
7.0		1									
		· ·									
B.O											
	1										
9.0					1						
	1	TC core drilling from 4.50m to 5.50m									
0.0		DC core drilling from 5.50m to 8.50m									,
	1										60
		ehole terminated at 8.50m									10,0
	**No	ote: SPT Conducted using winch cat-head device, N values rep	orted ar	e close t	o N ₇₀						17/ >

FIGURE 11 SOIL PROFILE AND SPT N VALUES AT BH 22 - M2

 PROJECT NO:
 SF/KI-48/Zone M2/PMPKM

 BORE HOLE NO:
 BH/22

 Date of start
 : 23-Mar-2013

 Date of finish
 : 23-Mar-2013

MIG Tenements, TNSCB, Chennai Perumbakkam, M2 Zone ates ; Block M11

Project

Co-ordinates

Site

GWL from GL : 1.00m Ground level RL : 1.267m

GL(m)	Soil Profile		Dept sam		T		SPT	/ VST			RD/
딁	Ē.	ield Description	colle		Test depth		SPT	blow	cour	nts	Consistency
I	S		UDS	DS	m	15	30	45	60	N**	
.0 1.3		Yellowish grey silty clay		0.50 0.75	0.75	1	1	2	2	3	Soft to medium stiff
2.6		Dark grey soft clay with reddish brown patches		1.50	1.50	Su	nk @	SPT	wt	0	Very soft
3.4		Black organic sandy clay		2.75	2.75	@	SPT	l wt ¦	1	0	Very soft
1.0		Dark greenish grey dirty fine to medium sand		3.50	3.50	3	8	9	23	17	Loose
4.8		Dark brownish grey dirty fine to coarse sand with weathered stones		4.50	4.50	35	50/8	 Bom		>100	Very dense
5.6		Brownish grey dirty fine to coarse sand with weathered stones	, , ,		5.50	Reb	oun	d d	1	RB	Very dense
i.0		Brownish grey highly weathered fractured rock	5.50-6.7	0	TC core						Very weak
6.7 7.0	3533			·	6.70					RB	
		Brownish and grey highly weathered severely jointed	6.70-7.7	0	Diamor recover		e dri	lling 1	VX siz	£ 0 ,	
3.0	等	rock	7.70-8.7	70	Diamor recove					ze,	Weak
9.0	60 65 60 60 60 65 60 60 60 65 60 60 60 60 60 60		8.70-9.7	70	Diamor					ze,	88.00.000
0.0		Br and grey weathered closely jointed rock		Ι	100070	, .c	10, 11.	T	ī	T	Moderate
1.0							:			1	
2.0											
3.0											
4.0											
					İ						
5.0											
6.0											
_	1										
7.0	1										
8.0											
<u> </u>	1										
9.0	1										
		TC core drilling from 5.50m to 6.70m									
0.0	1	DC core drilling from 6.70m to 9.70m									
	1		1	L	1	1		ĺ.,]	<u> </u>	1

FIGURE 12 SOIL PROFILE AND SPT N VALUES AT BH 23 - M2

 PROJECT NO: SF/KI-48/Zone M2/PMPKM

 BORE HOLE NO:
 BH/23

 Date of start
 25-Mar-2013

 Date of finish
 25-Mar-2013

 GWL from GL
 1.00m

1.200m

Ground level RL

Project MIG Tenements, TNSCB, Chennai Site Perumbakkam, M2 Zone

Co-ordinates : Block M12

Diameter and type of boring ; 150mm Rotary boring with drilling mud circulation

SPT / VST Depth of Soil Profil Depth froi GL(m) samples RD/ Test Field Description SPT blow counts collected Consiltency depth UDS DS m 15 30 45 60 N** Yellowish grey silty clay 0.50 Medium stiff 0.6 1.0 @SPT wt 0 0.75 0.75 1 Light brownish grey soft silty clay with yellow patches Very soft Sunk @ SPT wt 0 1.50 1.50 2.0 2.25 2.25 Sunk @ SPT wt 0 Dark grey very soft silty clay with medium sand 3.0 Very soft patches and decayed wood 3.00 3,00 0 1 2 25 3 3.5 3.75 3.75 50/15cm >100 4.0 Dark yellowish grey dirty fine to coarse sand Very dense weathered stones >100 4.50 4.50 30/6cm 5.0 Dark yellowish grey completely weathered fractured Very weak RB 5.50 Rebound 5.5 TC core drilling 6.0 Yellowish grey highly weathered fractured rock 5.50-6.30 Very weak 6.30 Rebound RB 6.3 Diamond core drilling NX size, 6.30-7.30 7.0 recovery 8%, RQD nil Brownish and grey weathered severely jointed rock Weak Diamond core drilling NX size, 7.30-8.30 8.0 recovery 12%, RQD nil 9.0 10.0 11.0 12.0 13.0 14.0 15.0 16.0 17.0 18.0 19.0 TC core drilling from 5.50m to 6.30m DC core drilling from 6.30m to 8.30m 20.0 Borehole terminated at 8.30m **Note: SPT Conducted using winch cat-head device, N values reported are close to N₇₀

FIGURE 13 SOIL PROFILE AND SPT N VALUES AT BH 24 - M2

PROJECT NO: SF/KI-48/Zone M:2/PMPKM BORE HOLE NO: BH/24

26-Mar-2013

MIG Tenements, TNSCB, Chennai Date of start

Site Perumbakkam, M2 Zone Co-ordinates ; Block M12

Project

Diameter and type of boring : 150mm Rotary boring with drilling mud circulation

Date of finish : 27-Mar-2013 GWL from GL : 1.00m Ground level RL : 1.295m

r		7,50 0, 00,110	1		Ciodila						
E ~	offle		Dept				SPT /	VST	· 		
Depth from GL(m)	Soil Profile	Field Description	, sam colle		Test		SPT	blow	cour	nts	RD / Consistency
De De	Soil		UDS	DS	depth m	15	30	45	60	N**	Consistency
		Yellowish grey silty clay	350	0.50		٦		-7-3	30		Soft
0.5				0.50							.001
1,0		Light brownish grey soft silty clay with few stones	1	0.75	0.75	Su	nk @	SPT	wt	0	Very soft
1.8			4.50			•					10,700.
2.0		Light grey soft silty clay	1.50	l		l	<u> </u>				Very soft
2.8		Yell grey dirty fine to coarse sand with w. stones		2.00 2.75			PTwt	20	33	20 >100	Very dense
3.0		Yellowish grey highly weathered fractured rock	2.75-3.3							i	
3.4		renowish grey riightly weathered fractured fock	2.70-0.0				ound			RB	Very weak
4.0			3.30-4.3	30	Diamor					e,	
3		Light grey and light brown weathered severely			recover	y 197	%, KQ	DIII			Weak
5.0		jointed rock	4.30-5.3	10	Diamor					e,	
					recover	y 24%	%, P.Q	D níl			
6.0											
7.0											
8.0											
0.0											
9.0											
10.0				 							
11.0				•							
						1					
12.0		·									
13.0											[
14.0											
15.0				ĺ	[
10.0											
16.0											
16.0											
	•	•									
17.0											,
			ļ.								
18.0			-								
					İ						
19.0			•		}						
	1	TC core drilling from 5.00m to 6.30m									
20.0		DC core drilling from 6.30m to 8.30m									
]							09.
		hole terminated at					·				107
	**No	te: SPT Conducted using winch cat-head device, N values rep	orted are	close to	N ₇₀						

	GWL 0.00m RL			FIGURE 14 SUB-SOIL PROFILE BH/13 – BH/14 – BLOCK M-7 TNSCB TENEMENTS AT PERUMBAKKAM
BH/14	N S	25 28 27 20 27 20 27 20 27 27 27 27 27 27 27 27 27 27 27 27 27	8 4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	SUB-5
BH/13	10 Yellowish grey silty day with roots and few stones 25 Grevish brown / vellowish grey sandy clay with stones	00 Gre	RB R0 Brownish grey highly / completely weathered severely jointed rock R13 Yellowish grey and grey highly weathered and severely jointed rock	NOTES: NOTES: Notes fevations with respect to the site reference datum. Ground water table is from the boreholes
	1.0	уи IN METRES		NOTES The ground water table

BH/16	**	10 GWL 0.00m RL	19 min 19	82 ->100		RB	ανίν Qu / completely weathered R-13		coarse sand with weathered stones	R-16 C-0 severely jointed rock	FIGURE 15 SUB-SOIL PROFILE BH/15 - BH/16 - BLOCK M-8 TNSCB TENEMENTS AT PERUMBAKKAM	
BH/15	N" Valouish aray / brownish aray silty clay with reets	e insansanan	Greyish brown clayey silty fine to coarse sand with gravel and sandy clay lumps	RB Coarse sand with weathered stones	ନ୍ଦ୍ର Ro Brownish grey highly weathered fractured rock	F 0-0	Brownish grey completely weathered severely jointed rock Yellowish grey highly calcareous sandstone	Greyish partly weathered closely jointed rock	Brownish grey dirty fine to	Greyish partly weathered	NOTES * NOTES * The ground plevations with respect to the site reference datum. Ground water table is from the boreholes	42
	2.0	0.0	1.0	ETRES		4.0	-5.0	0.6	-7.0	0. 0,	NOTES * The ground Mare rable	Maria Chian

		GWL			red stones					FIGURE 16	SUB-SOIL PROFILE BH/18 - BH/17 - BLOCK M-9 TNSCB TENEMENTS AT PERUMBAKKAM
	Yellowish grey / brownish grey silty clay with roots	hes	Dark grey soft sity clay with	Greyish / brownish clayey silty fine to coarse sand with sandy clay lumps	Yellowish grey / brownish grey clayey silty fine to coarse sand RB with weathered stones	Yellowish grey / dark greenish grey highly weathered fractured rock	Greyish brown and grey completely Re weathered severely jointed rock R49	Gνownish and grey highly weathered severely jointed rock			SAUS
BH/18	********************	2	8 Yellowish and brownish grey silty Clay	-1.0 Greyish / bro	-2.0	-3.0	87 8.7 8.7 8.7 8.7 8.7 8.7 8.7 8.7 8.7 8		-8.0 -9.0		NOTES: (The ground electrons with respect to the site reference datum.

Brownish grey with gravel and sand 1.0 Brownish grey with reddish brown patches 2.0 Brownish grey with gravel and sand 1.0 Brownish grey soft silly clay with gravel and sand 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.	·			
1.0 Brownish greey Sifty day with grevel and send belowish grey brownish grey soft silty day with reddish brown patches 2 Brownish greey Sifty day with gravel and send belowish grey brownish grey soft silty day with reddish brown patches 2 Brownish greey Sifty day with gravel and send belowish grey brownish grey brownish grey silty fine to coarse send with weathered stones 2 A D Yellowish grey / brownish grey brownish grey brownish weathered stones 2 A D Yellowish grey / brownish grey		BH/20	B	И9
Brownish grey Light grey and yellowish grey soft silty clay with reddish brown patches 0 1. 1.0 1. 1.0 1. 1.0 1. 1.	2.0-	ž		¥
Brownish gray 10 Light gray and yellowish gray soft silty clay with reddish brown patches 0 1.0	1.0	Yellowish grey / bre	ownish grey silly clay with roots	A CAMPAGE AND A
Brownish grey sity fine to stip clay with gravel and sand sand sand sand sand sand sand	0.0	0 Light grey and yellowi	ish grey soft silty clay with reddish brown patches	GWL GWL
2.0 RB Yellowish gray / brownish gray lity fine to coarse sand with weathered stones with weathered stones and with weathered stones with weathered stones with weathered fractured rock RB RB Fig. Yellowish gray / brownish gray highly weathered closely / severely BB Fig. Coarse sand with weathered stones RB BB Fig. Coarse sand with weathered stones RB BB Fig. Coarse sand with weathered stones RB BB Fig. Coarse sand with weathered stones rock (sitistone) BB Fig. Coarse sand with weathered stones rock fig. Coarse sand with weathered stones rock fig. Coarse sand with weathered stones rock fig. Coarse sand with weathered stones rock fig. Coarse sand with weathered stones rock fig. Coarse sand with weathered stones rock fig. Coarse sand with weathered stones rock fig. Coarse sand with weathered stones rock fig. Coarse sand with weathered stones rock fig. Coarse sand with weathered stones rock fig. Coarse sand with weathered stones rock fig. Coarse sand with weathered stones rock fig. Coarse sand with weathered stones rock fig. Coarse sand with weathered stones rock fig. Coarse sand with weathered stones rock fig. Coarse sand with weathered stones rock fig. Coarse sand with weathered stones rock fig. Coarse sand with weathered stones rock fig. Coarse	5 ,	10 Brownish grey silty clay with gravel and sand		
RB Yellowish gray / brownish gray highly weathered fractured rock RB RB A Yellowish gray / brownish gray highly weathered fractured rock RB RB A Light brown and grey widely jointed rock (siltstone)		24	rey / brownish grey clayey silty fine to coarse sand with weathered stones	44
RB R12 1-50 4.0 1-50 8.0 1-5		RB Vollawich gray / brown	nich grav highly weathered fractured rock	>100 RB
6 4.0 RA12 Light brownish grey /brownish weathered closely / severely RA19 jointed rock (siltstone) GA28 Light brown and grey widely jointed rock (siltstone) RA19 GA28 CA28 Light brown and grey widely jointed rock (siltstone) GA28 CA28 CA28 CA28 CA28 CA28 CA28 CA28 C			() () () () () () () () () ()	
-5.0 -7.0 -8.0 -9.0 -9.0 -9.0 -9.0 -9.0 -9.0 -9.0 -9			grey /brownish weathered closely / severely jointed rock (siltstone)	F19
-9.0 -9.0 -9.0 -9.0 -9.0 -9.0 -9.0 -9.0		Q.25	ely jointed rock (siltstone)	R31
-9.0 -9.0 -9.0 -9.0 -9.0 -9.0 -9.0 -9.0	-6.C-			
NOTES: Note with respect to the site reference datum.	.0. 6.0.			
NOTES: And still respect to the site reference datum.	Ö,			
NOTES: (1) NOTES: (1) Note of the site reference datum.		09:		
NOTES: (F)		Y97.		FIGURE 17
Section of the parent of the p	₹ ₹	is a state of the site reference datum.		SUB-SOIL PROFILE BH/20 - BH/19 - BLOCK M-10 TNSCB TENEMENTS AT PERUMBAKKAM

BH/22	3 GWL 0.00m RL 0.0000 RL 0.000m RL 0.0000 RL 0	FIGURE 18 SUB-SOIL PROFILE BH/21 – BH/22 – BLOCK M-11 TNSCB TENEMENTS AT PERUMBAKKAM
	Yellowish grey soft silty clay with yellow patches Light grey and dark grey soft silty clay with reddish brown patches Light grey and dark grey soft silty clay with reddish brown patches Black organic sandy clay With sandy clay lumps Coarse sand with weathered stones Yellowish grey / brownish grey / brownish grey In highly weathered fractured rock Brownish and grey weathered and closely jointed rock Brownish and grey weathered and closely jointed rock	re site reference datum.
BH/21	1.0 0.0 1.0 0.	NOTES: The ground elevations with respect to the site reference datum. Ground water table is from the boreholes

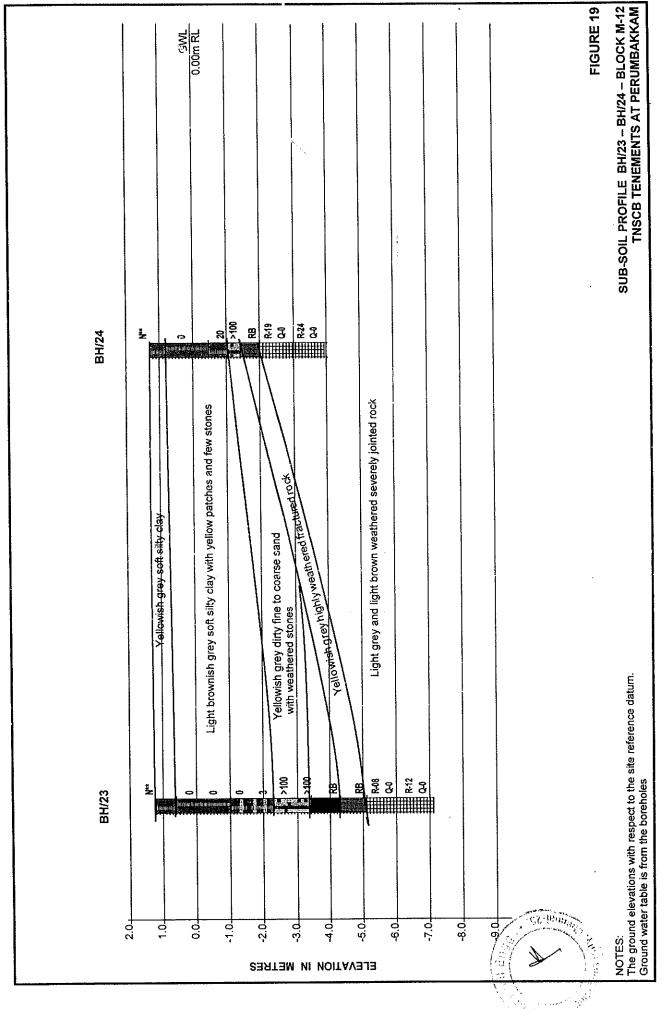


TABLE 1 LABORATORY TEST RESULTS OF SOIL SAMPLES OF BH 13 - M2

MIG Tenements, TNSCB Perumbakkam

Borehole Nos: BH13

Project:

Type of Boring and dia of bore hole: 150mm diameter rotary boring with mud circulation

Depth	Depth Type	Description	Ž	CLASS NMC	NMC		님	ā	5	FSI	SG	9	SS	MS	FS	Silt	Clay
Ξ	(2)	(3)	4	(2)	(9)	8	(8)	(6)	(10)	(11)	(12)	(13)	(14)	(31)	(16)	(17)	(18)
		ROREHOI F BH13															
GL-0.5(SO	GL-0.50 DS Yellowish grey silty clay with few stones			22.1				,	45.4						·	
0.75		SPT Yellowish grey silty clay with gravel and stones	9	당	33.9	83.3	24.3	59.0	59.0 0.163 81.8	81.8							
1.50		SPT TOP: greyish brown sandy silty clay with stones	25	SC/CI	23.8	65.6	22.6	43.0	43.0 0.028 100.0	100.0							
		BOT: Greyish brown clayey silty sand with coarse particles			13.2				· · · ·	•							
2.25		SPT Greyish brown clayey silty fine to coarse sand with sandy clay lumps	47	SC/SM	19.1							2.7	15.1	36.3	56.9	19.0	
3.00		SPT Greyish brown dirty fine to coarse sand with weathered stones	>100	SC/SM	23.9						•	2.0	16.6	36.3	24.7	20.4	
3.75		SPT Greyish brown dirty fine to coarse sand	>100		17.1					,							
4.50	SPT	SPT Greyish brown dirty fine to coarse sand with weathered stones (wdr)	>18		4.5.4									-			
7.30	7.30-8.30	Brownish grey highly weathered severely jointed rock															
				•													
																_	



TABLE 2 LABORATORY TEST RESULTS OF SOIL SAMPLES OF BH 14 - M2

MIG Tenements, TNSCB Perumbakkaın

Project: MIG Tene Borehole Nos: BH14

Type of Boring and dia of bore hole: 150mm diameter rotary boring with mud circulation

4	1	Description	į,	CLASS NMC	NMC	F	곱	直]	FSI	SG	ຶ່ນ	SS P	MS	FS Silt	It Clay
<u>a</u>	nebul 1 ype	107	9	<u>(0</u>	9	8	@	6	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17) (18)
€ —	8	(2)	E	ĵ.		7		┿	┿~	ᅩ	+-		-	\vdash		_
		BOREHOLE BH14					***************************************									
GL-0.50	DS	GL-0.50 DS Yellowish grey silty clay with roots		万	29.4	82.8	21.5	61.3 0.129 191.6	129	191.6						
0.75	SpT	0.75 SPT Yellowish grey sifty clay	သ	ᆼ	32.9	85.3	24.3	24.3 61.0 0.141 66.6	7.141	9.99			<u> </u>			
1.50	SPT	1.50 SPT Yellowish grey silty clay with white stones and gravel	17	동	35.7	85.3	24.4	60.9 0.186 141.6	7.186	141.6						
2.25		SPT Greyish brown clayey silty sand with sandy clay lumps & weathered stones	25	SC/SM	20.3							2.0	9.5	26.7	31.6	30.2
3.00		SPT Grevish brown dirty fine to coarse sand with weathered stones	82		13.6											— <u>;</u>
3.75	SPT		×100	SM	16.4					-		9.5	17.0 3	33.0	24.7	
4.50	SPT	-	×100		14.9											
5.70	-6.70	5.70-6.70 Greyish brown highly weathered severely jointed rock												_		
6.70	6.70-7.70	Greyish brown highly weathered severely jointed rock														
7.70	7.70-8.70	Brownish grey highly weathered closely jointed rock (Granitic gneiss)														
.,																
										1	7	1		1	$\frac{1}{2}$	-



TABLE 3 LABORATORY TEST RESULTS OF SOIL SAMPLES OF BH 15 - M2

MIG Tenements, TNSCB Perumbakkam Project:

Borehole Nos: BH15

Type of Boring and dia of bore hole: 150mm diameter rotary boring with mud circulation



TABLE 4 LABORATORY TEST RESULTS OF SOIL SAMPLES OF BH 16 - M2

Project: MIG Tenements, TNSCB Perumbakkam

Borehole Nos: BH16

Type of Boring and dia of bore hole: 150mm diameter rotary boring with mud circulation

Depth Type	Type	Description	"N"	CLASS NMC	NMC		ᆲ	豆	3	<u> </u>	ဗ္ဗ	ტ	g	SE	S.	ii iii	Clay
£	(2)	(3)	(4)	(5)	(9)	6	8)	6	(10)	3	(12)	(13)	(14)	(15)	(16)	3	38
														`			
		BOREHOLE BH16												1		~~~~	
05 0- 15	C.	GI-0-50 DS Yellowish arev silty clay (dv)			15.0					,			•				
0.75	SPT	SPT Yellowish grev silty clay with brown patches	5	G	30.6	84.2	21.5	21.5 62.7 0.145 86.9	0.145	86.9	***************************************			****			
50		SPT Yellowish grey and brown silty clay with few stones	19	CH	33.9	88.1	23.9	64.2	0.156 138.4	138.4		·····					
2.25	SPT	SPT Yellowish grey clayey silty sand with sandy clay lumps	4	SC/SM	19.8								ත ල	44.4	29.2	- 53	22.5
3.00		SPT Brownish grey dirty fine to medium sand with sandy clay lumps	82		12.4										***********		
3.75	SPT	3.75 SPT Greyish dirty fine to coarse sand with weathered stones (wdr)	×18	SW/SP	11.3							5.	21.6	50.5	18.1	8.3	ti.
5.80-	6.80	5.80-6.80 Yellowish grey highly / completely weathered calcareous sandstone					·										
6.80-	7.80	6.80-7.80 Brownish grey completely weathered granitic gneiss / sandstone															
8.30	SPT	8.30 SPT Brownish grey dirty fine to coarse sand with weathered stones			13.1												
9.20-1	10.20	9.20-10.20 Greyish partly weathered and severely jointed rock															



TABLE 5 LABORATORY TEST RESULTS OF SOIL SAMPLES OF BH 17 - M2

Project: MIG Tenements, TNSCB Perumbakkam Borehole Nos: BH17

Type of Boring and dia of bore hole: 150mm diameter rotary boring with mud circulation

Depth Type	Type	Description	N.	CLASS NMC	NMC	Ⅎ	급	ā	J	ES.	SG	ڻ ن	છ	SM	S.	<u></u>	Clay
Ξ	(2)	(3)	4	(5)	(9)	(2)	(8)	(6)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
		The state of the s															
												·····				•••	
											•	·w··					·
GL-05		DS Brownish grey silty clay with sand		SC-CH	17.5	17.5 58.4	19.5	38.9	38.9 <0.00 70.0	70.0							
0.75	SPT	SPT Brownish grey soft silty clay	0	문	70.0	95.6	26.8		68.8 0.628	83.0							
1.50	SPT	SPT Dark grey soft silty clay with gravel and organic material	0	S	54.8		77.3 25.8	51.5	51.5 0.563	55.0							
2.25		SPT Greyish clayey silty fine to coarse sand with weathered stones	88	SC/SM	16.0							9.1	15.8	29.2	27.7	25.7	_
3.00		SPT Brownish grey clayey silty fine to coarse sand with weathered stones	4	SC/SM	15.8							5.1	19.1	29.8	24.6	21.4	-
3.75		SPT Brownish grey clayey silty fine to coarse sand	×100		18.5					•							
7.0-	7.0-8.0	Brownish and light yellowish fully weathered severely jointed rock															
8.0-	8.0-9.0	Yellowish grey and grey highly weathered severely jointed rock															

									┨							1	\neg

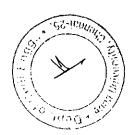


TABLE 6 LABORATORY TEST RESULTS OF SOIL SAMPLES OF BH 18 - M2

Project: MIG Tenements, TNSCB Perumbakkam

Borehole Nos: BH18

Type of Boring and dia of bore hole: 150mm diameter rotary boring with mud circulation

Depth Type	Type	Description	ž	CLASS NMC	NMC	17	Ъ	ld	i	FSI	SG	9	ငး	MS	FS	Silt C	Clay
ε	(2)	(3)	(£)	(2)	(9)	3	(8)	(6)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
										<u> </u>							
		BOREHOLE BH18												- इ			
														*			
GL-0.50	മ	GL-0.5d DS Yellowish grey silty clay with black patches		ۍ	19.9	57.4	17.5		39.9 0.060 60.0	60.0	*************						
0.75	SPT	SPT Brownish grey silty clay with reddish brown patches	7	£	38.1	74.1	21.6	52.5	52.5 0.314 108.0	108.0							
1.50	SPT	SPT TOP: Yellowish grey and brownish silty clay	œ	£	29.5	71.3	21.4		49.9 0.162	54.5							
		BOT: Brownish clayey silty fine to medium sand			21.3												
2.25	SPT	SPT Brownish clayey silty fine to medium sand / sandy silty clay	24	သွ	18.9					<u></u>	1.8	-	6.1	22.3	36.5	33.3	
3.00		SPT Greyish brown dirty fine to coarse sand with weathered stones	74	SM	13.7							9.7	17.5	31.2	27.1	14.5	
3.75	SPT	3.75 SPT Yell grey clayey silty fine to coarse sand with weathered stones (wdr)	>100	SP/SiM	13.7							28.7	24.6	21.0	13.1	12.6	
5.50-	6.50	5.50-6.50 Greyish brown & grey completely weathered severely jointed rock							•	····							
6.50-	6.50-7.50	Brownish and grey highly weathered severely jointed rock									··········						
7.50-	7.50-8.50	Brownish and grey highly weathered severely jointed rock															
				VIII							···········						
					,,,,,,,								_	_		_	



TABLE 7 LABORATORY TEST RESULTS OF SOIL SAMPLES OF BH 19 - M2

MIG Tenements, TNSCB Perumbakkam

Borehole Nos: BH19

Project:

Type of Boring and dia of bore hole: 150mm diameter rotary boring with mud circulation

LI FSI SG G CS MS FS SII	3		****	45.5 0.215 70.0	44.7 0.450 115.0	13.4 28.1 0.762 23.8	200	ţ.					
Ī		+	-William -	45.5	44.7	28.1			.viin				
ā		9		19.9	17.0	13.4							
=	1 6	1		65.4	61.7	41.5	****						
CMN CMN		6		29.7	37.1	34.8	19.0	15.6	16.7	13.9			
OMN SS IO) ((c)		동	끙	ច		SP/SM		SP/SM			
11/411	Z (4)			7	0	31		4	×190			
	Description	(3)	BOREHOLE BH19	The many city clay with brown and black patches	GL-U.5U DS BIOWINSI grey sink clay with reddich brown patches	SPI (Yellowish grey sont slint clast with reddish brown patches	SPT TOP: Greyish sandy clay with gravel / clayey sand with gravel	BOT: Brownish grey dirty fine to coarse sand	SPT Brownish grey dirty fine to coarse sand weathered stones	3.75 SPT Brownish grey dirty fine to coarse sand with weathered stones	5.50-6.50 Brownish highly weathered severely jointed rock (slitstone)	6.50-7.50 Light brownish and light grey widely jointed hard rock (siltstone)	
- 1					<u>ہ</u> ا	- <u>+</u>	- <u>-</u>		<u></u>	F	_	_	
	Depth Type	(2)		_ 6	<u>ვ</u>	0.75 SF	1.50 SP 2.25 SP		3.00 SF	S	- - - - - -	-7.5(



TABLE 8 LABORATORY TEST RESULTS OF SOIL SAMPLES OF BH 20 - M2

MIG Tenements, TNSCB Perumbakkam

Borehole Nos: BH20 Project:

Type of Boring and dia of bore hole: 150mm diameter rotary boring with mud circulation

			Ž	CLASS NMC	NMC		14	<u>-</u>	=	FSI	SG	<u>ຶ</u>	CS M	MS	FS S	<u> </u>	Clay
Depth Type	Туре	Description		(6)	6	<u> </u>	<u>@</u>		(10)	(3)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
3	(5)	(3)	Ē		1	1		-	T	-	-						
		BOREHOLE BH20															
	Č	العام بالماء بمعتم بالمادية		ᆼ	28.9	61.1	18.2	18.2 42.9 0.249 70.0	0.249	70.0							
-1-0.3 -1-0.3	3	פאלילפית מייינים אליהייינים אינייים פאלילפית מייינים אליהייינים אליהייים בייינים אליהייים אליהייים אליהיים אליהייים אליהיים אלים אליהיים אליהיים אליהיים אליה אליהיים אליהיים אליהיים אליהיים	0	동	38.5	65.8		17.8 48.0 0.431 27.0	0.431	27.0							
0.75	SPT	0.75 SPT Light grey very soft slift clay with reddish blown parches	Ç	5	30.4	71.8	22.8	71 8 22 8 49.0 0.155 180.0	0.155	180.0							
1.50	SPT	1.50 SPT Brownish grey silty clay with gravel and sand	2 ;		- L	?				<u></u>		50	7.7	25.3 36.8	89.0	24.7	
2.25	SPT	SPT Yell grey clayey silty fine to med sand with stones & sandy clay lumps	24	NO-28	0 0							177	17.7 16.6 26.6	5.6	22.1	17.0	
3.00	SPT	3.00 SPT Yellowish grey clayey silty fine to coarse sand with weathered stones	•	SC/SM	12./								 				
4.80	-5.80	4.80-5.80 Light brownish grey weathered closely jointed rock									•						
5.80	5.80-6.80	Light brown and grey widely jointed hard rock (siltstone)															
									1	4	1	-					



TABLE 9 LABORATORY TEST RESULTS OF SOIL SAMPLES OF BH 21 - M2

MIG Tenements, TNSCB Perumbakkam

Borehole Nos: BH21

Project:

Type of Boring and dia of bore hole: 150mm diameter rotary boring with mud circulation

4		Description	į	CLASS NMC	NMC	11	김	ā		FSI	SG	0	SS	MS	FS	Silt	Clay
neptu	Deptin Spe	(3)	4	(2)	9	3	(8)	6)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	38
Ξ	<u> </u>							_		\vdash	-						
		BOREHOLE BH21															
ر د د	۲	Colored Nellowish arey medium stiff silty clay		균	22.2	64.4	18.4	46.0 0.083 80.0	.083	0.0							
77.0	3 5	CDT Vallowish arev soft silly clay with vellow patches	7	F	38.2	78.0	21.2	56.8 0.	0.299 175.0	75.0							
2 6		TOD: Lick and old old old with reddish brown patches	7		9.09							····					
00.1		TOT. Light gird soil saily only man order candy eith clay with praye		SC/CI	19.5	47.6	16.4	31.2 0.099	9 660	68.4							
		שניין המילול היי לייי לייי לייי לייי לייי לייי ל	77	MS/US							-	14.2 2	20.9 2	25.4 2	20.1	19.4	
2.25		SPT Yell grey clayey silty sand with sandy clay lumbs and weamered sturies	‡										<u>.</u>		_	22.0	_
3.00		SPT Yell grey clayey silty sand with sandy clay lumps and weathered stones	49	SC/SM								2 2 2	7.17	7.7	†	3	
3.75	SPT	3.75 SPT Yellowish grey clayey silty sand with weathered stones	>100		1 .3		· ,									•	
5.50)-6.50	5.50-6.50 Greyish weathered severely jointed rock															
6.50)-7.50	6.50-7.50 Greyish weathered severely jointed rock															
7.5(7.50-8.50	Brownish and grey weathered closely jointed rock											<u> </u>			***	
																,	
								-	\dashv	-	$\frac{1}{2}$		-	\dagger	1	1	Ì



TABLE 10 LABORATORY TEST RESULTS OF SOIL SAMPLES OF BH 22 - M2

MIG Tenements, TNSCB Perumbakkam Project:

Borehole Nos: BH22

Type of Boring and dia of bore hole: 150mm diameter rotary boring with mud circulation

(1) (2)				TOTAL OPEN	1	<u></u>	Σ	j	5	}	, ,)	- }	2		
(2)	(3)	4	(2)	<u>@</u>	6	8)	6)	(10)	(3)	(12)	(13)	(14)	(15)	(16)	(17) (18)
						T	T	 	_	<u> </u>	\vdash	_			
	BOREHOLE BH22													,	
GL-0.50 DS	GL-0.50 DS Yellowish grey silty clay		ᆼ	20.4	66.8	20.3	46.0 <0.00 80.0	00.0≻	80.0						
TGS 270	SPT Yellowish grey silty clay	က	퓽	34.2	75.3	21.2	54.1 0.240		90.0						
	SDT Dark may soft clay with reddish brown patches	0	공	68.5	104.7	30.9	73.8 0.509		9.99						
	Total grands conditions and the second secon	0		42.6						*****					
	Diach August Sasial way	17	WS/OS	17.8						- ~	3.9	13.8	38.4	23.8	20.1
3.50 SP1	SPI Dark greenish grey dirty line to medium samu	-		?						_				9	0
4.50 SPT C	SPT Dark brownish grey dirty fine to coarse sand with weathered stones	>100	SW/SP	14.6						4	7.1.7	0.07	32.2	<u>.</u>	; –
7.70-8.70 E	Brownish and grey highly weathered severely jointed rock				.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,										
8.70-9.70 E	Brownish and grey weathered closely jointed rock														
	-														
												\dashv		-	\dashv



TABLE 11 LABORATORY TEST RESULTS OF SOIL SAMPLES OF BH 23 - M2

Project: MIG Tenements, TNSCB Perumbakkam Borehole Nos: BH23

i D D	200	BOYENDE NOS. DILL.	10+10				Grou	W bu	Ground Water Table:	ple:	8	n to 1.	1.00m to 1.40m, March- April 2013	March	- April	201	_[
Type	of Borit	r rotary boring with mud circuit		CIASS NMC	CMZ	=	립	己	=		SG	<u>ບ</u>	SS	MS	FS	Silt	Clay
Dept	Depth Type	Description	ζ.	5			<u> </u>		. ;				- 3		(38)	7	(48)
-		(3)	₹	<u>(</u> 2	<u>@</u>	8	<u>@</u>	<u>ල</u>	(10)	(11)	(71)) (?;)	(14)) (c:)	-+	_	<u>.</u>
£	(2)								-								
		ROBEHOLE BH23															
							1	-	- 0					-			
				끙	26.7	64.2	20.8	43.4	43.4 0.135 90.0								
GL-0.50	2	US Tellowish grey siny clay		;	i	6	7	000	3070	22.2							_
7		CDT I in the brownish grey soft silts clay with vellow patches	0	5	ο. Ο.	7.55	24.3	2.0	3	?		_					
			c	Ç	9	04 0 1100 6	26.8	73.8 0.911	0.911								
4 50		SDT I intrownish grey very soft clay with yellow patches	>	5	?	2	;	:	:				_				
<u>.</u>			c	Ç	7.7.1	58.9 15.7	15.7	43.2	43.2 0.912 70.0	70.0							-
2.25		SPT Dark grey very soft silty clay with medium sand patches	>	5	 }								42.2	30.6	25.4	22.5	
		TOD: Dark orev sandy clay with coarse particles	ო	သွ	24.0								2.2			-	
3.00				-	2889												
		MID: Decayed wood			2.22							- 0			-	16.7	
		Sends barathaw bres earned of one will be a send of the send of th		SM	12.3							0.0	0.0	- 7	- - -	:	
		BOT: Dark greenish grey unity line to coarse saile wearrened exercise	•	(1							13.5	15.3	29.9	27.4	13.9	
3 75	SPT	SPT Dark vellowish grey dirty fine to coarse sand weathered stones	×199	SM/SF	11./			•)				-	
	i 	000000	7100		13.4				-								
4.5	SPT	4.50 SPT Dark yellowish grey dirty fine to medium sand with weathered stories	3		<u>.</u>												
<u>`</u>	7 20	control Design and grav weathered severely jointed rock					****			-							
	0.7-00	ביים מונים לוכל אכתיים ביים ליים ליים ליים ליים ליים ליים ל								_						_	
7.	7.30-8.30	Brownish and grey weathered severely jointed rock							•								
	_																
													-				
	_												Ì				



TABLE 12 LABORATORY TEST RESULTS OF SOIL SAMPLES OF BH 24 - M2

Project: MIG Tenements, TNSCB Perumbakkam Borehole Nos: BH24

Boret	ole No	Borehole Nos: BH24					Ċ	707	7 T	Ozorad Motor Toble:	100	50 T	40m	March	1 00m to 1 40m March- Anril 2013	2013	~
Type	of Boril	Type of Boring and dia of bore hole: 150mm diameter rotary boring with mud circulation	ation		ļ		5	אַ מון	121		3	3	}	5			
	Don't Type	Description		CLASS NMC	NMC	<u></u>	립	<u>a</u> .		S.	_ წ	<u> </u>	<u>က</u> လ	MS	Տ	ა_ #8	Ciay Ciay
<u> </u>) y		Ð	(5)	9	9	8	6	(10)	(11) (12)		(13)	(41)	(15)	(16)	(17)	(18)
€	(2)	(5)		2		1	┿	-						\mid	_	-	Γ
		BOREHOLE BH24		. 				····								·····	
	Č	Vellounieh grav eith Clav		동	22.3	22.3 66.3 20.2 46.1 0.046 100.0	20.2	46.1	0.046	0.00							
קריי	3			į	5		0	7 7 93	0 5/ // // // // //	9			_				
0.75		SPT Light brownish grey soft silty clay with few stones	>	5	25.3	3.5.2		<u></u>	<u> </u>	 ?		·····					
-		Senote weith with season some definition of the Control of the Senote with few stones.			55.6												
 		I OF. Eight blownian grey sort sind old min ton come					1		í								
		BOT: Light grey soft sifty clay		당	85.7	85.7 83.3 23.2 60.1 1.070 70.0	23.2		.070	70.0							
			20		90.6												
2.00		SPI TOP: GreyIsri Soit Sity day	i					·····				_	1			2.0	
		BOT: Yellowish grey dirty fine to coarse sand with weathered stones		SC/SM	16.6						·, .	 ກຸ	7.02 7.21		20.6	· -	
2.75		SPT Yellowish grey highly weathered fractured rock	2100							•							
3.3	04.30	3.30-4.30 Light grey and light brown weathered severely jointed rock															
4.3	0-5.30	4.30-5.30 Light grey and light brown weathered severely jointed rock															
	_														, ,		
				_					1	1	1	1	1	1	$\left \right $	$\frac{1}{2}$	1



TABLE 13 SHEAR STRENGTH PARAMETERS FOR DIFFERENT LAYERS - M2 TNSCB, MIG, PERUMBAKKAM, Ground water table = 1.00m to 1.40m (March-April 2013)

	Soll	z	Design N"	Design N" Angle of friction	Shear Strength cu	Ы%	Compressibility
Below GL		100			c. = 5.0 t/m ²	59	$m_{\nu}=1/(42N)m^2/t$
0.00m to 1.30m	valuate grey silty clay with few stones, Ll = 0.163	2	2		. :	(4) Card M M M M M M M M M M M M M M M M M M M
		25	25		േ≈12 V™	43	111/-T/(++1/)/T-/11
1.30m to 1.90m	Greyish brown sandy silty clay with stones, $L! = 0.020$	ì	į	1			C using a = 26 N t/m2
	Sandy clay jumps	47	45	./>n ⇔			
1.90m to 3.20m		9	000	A= 12°			C using q _c = 30 N t/m ²
2 20m to 5 50m	Greyish brown dirty line to coalse salid with medicine constraints	2700	207	1			
110000001107	disintegrated rock)	0	000		$c_u = 100 \text{ t/m}^2$		C using qo= 35 N t/m²
5 50m to 6.30m	Yellowish grey highly weathered fractured rock	ā	2				
	solution in the second second second solution to the second secon						
6.30m to 8.00m	Brownish grey fightly / Completely weathered 50-00-00 journal of the present bights weathered severely jointed rock						
Roreh	Borehole BH14 (GL = 1.451m RL)						
		7	N apiaon	Anote of friction	Shear Strength	Ы %	Compressibility
Depth	Soil	z	N LIXISACI	المتعدد المتعدد	ກິວ		
Below GL		L	2		$c_0 = 3.0 \text{ t/m}^2$	61.3	mv=1/(42N)m²/t
0.00m to 1.40m	Yellowish grey silty clay with roots in the top 0.40m, LI = 0.129 to 0.141)		- 7 E + /m2	0	m ₂ =1/(42N)m ² /t
000	Vollawish gray silty clay with white stones and grave!, Ll = 0.186	17	15		- 1:1 / C. / = 00	9	C
1.40m to 2.20m	בפונסאופון פונא פוויל פוני נייניי בייניי פוניים פוניים פוניים פוניים פוניים פוניים פוניים פוניים פוניים פוניים	20	25	ф = 32°			C using qo≠ 22 N Vm²
2,20m to 3.00m	Greyish brown clayey sifty sand with sandy clay lumps & weamered stories	}	;				C using at 24 N t/m2
W 00 F + + + 00	Cravich brown dirty fine to coarse sand with weathered stones	82	50	φ = 40°			
3.00m to 4.00m	מופלופות מונית ליונית ליונית ליונית מונית ליונית מונית ליונית מונית ליונית 4	100	6 = 42°			Cusing qe= 26 N Vm²	
4,00m to 5.00m	Brownish grey dirty fine to coarse sand with weathered stones	200	3 4	! }	- 100 +/m ²		C using a= 35 N t/m2
5 00m to 5 70m	Grevish brown highly weathered fractured rock	SB B	200		20 1 20		
	Slocy bestrict standard from the second						
5.70m to 8.20m							
8.20m to 9.00m	Brownish grey highly weathered closely jointed rock (Granitic gneiss)						
Boreh	Borehole BH15 (G) = 1.339m RL)						
1000	VIV. CITES AND THE CONTRACT OF						Compressibility
Depth Below GL	Soil	Z	Design N	Angle of friction	C _D	8	Compleasions
0.00m to 0.50m	Brownish grey silty clay with roots	ı	(1	63.0	mv=1/(42N)m²/t
0.50m to 1.70m	Yellowish grey silty clay, LI=0.145 to 0.156	00	xo		200	}	2m/+ IA AC T 2 Action 0
m)6 C of 1101 1	Gravish brown clayev sifty sand with weathered stones	21	20	φ = 32.0°			- in the state of
1.70m to 2.30m	משיין ייין ייין ייין ייין ייין ייין ייין	84 to >100	08 0	6 = 41°			C using $q_c = 26 \text{N} \text{Um}^2$
2.30m to 3.20m	Yellowish grey dirty fine to coarse sand with sandy clay lumps	 		.	$c = 100 \text{ t/m}^2$		C using $a_c = 35 \text{ N t/m}^2$
•	The state of the s	88	200		~ ^ ^ ^ ^ T		· · · · · · · · · · · · · · · · · · ·

Brownish grey completely weathered severely jointed rock Greyish partly weathered jointed rock (granitic gneiss)

Brownish grey highly weathered fractured rock

3.20m to 5.60m 5.60m to 6.80m 101 6280m to 7.70m

Engg.

Borehole BH16 (GL = 1.240m RL)

Depth	OAI	z	Design N	Angle of friction	Shear Strength pl	PI % Co	Compressibility	
Below GL 0.00m to 0.50m 0.50m to 2.10m 2.10m to 3.00m 3.00m to 3.80m 3.80m to 4.70m 4.70m to 5.80m 5.80m to 8.10m	Yellowish grey silty clay (dry) Yellowish grey silty clay (dry) Yellowish grey and brown silty clay with few stones, LI = 0.145 to 0.156 Yellowish grey and brown silty clay with sandy clay lumps Brownish grey dirty fine to medium sand with sandy clay lumps Greyish dirty fine to coarse sand with weathered stones (wdr) Brownish grey highly weathered fractured rock Yellowish grey highly / completely weathered calcareous sandstone Brownish grey dirty fine to coarse sand with weathered stones	10,19 41 82 >100 RB	12 40 80 100 200	φ	$c_u = 6.0 \text{ t/m}^2$ 6 $c_v = 100 \text{ t/m}^2$	63.0 T _V	$m_y=1/(42N)m^2/t$ C using $q_c=24 N t/m^2$ C using $q_c=26 N t/m^2$ C using $q_c=30 N t/m^2$ C using $q_c=35 N t/m^2$	1
9.20m to 10.20m	10.20m Greyish partly weathered and severely junical room Rorehole BH17 (GL = 1.492n) RL)							1
Depth Below G	H	z	Design N	Angle of friction	Sucal Suchight	٥ *ا	Compressibility	ŀ
0.00m to 0.50m 0.50m to 1.40m 1.40m to 2.30m 2.30m to 3.20m	Brownish grey silty clay with sand Brownish grey soft silty clay , LI = 0.628 Dark grey soft silty clay with gravel and organic material, LI = 0.563 Greyish clayey silty fine to coarse sand with weathered stones	0 0 38 41, >100	4 4 8 00 20 00			68.8 51.5 0	C using $q_0=24 \text{ N t/m}^2$ C using $q_0=24 \text{ N t/m}^2$	
4.20m to 6.00m	Dark greenish grey completely weathered fractured rock	RB	200	in the second se	c, = 100 Vm²		مد مد مد مد مد مد مد مد مد مد مد مد مد م	- 1
Boreh Boreh	Borehole BH18 (GL = 1.409m RL)	Z	Design N	Angle of friction	Shear Strength	PI % Id	Compressibility]
Below GL 0.00m to 0.50m 0.50m to 1.40m	Yellowish grey silty clay with black patches Brownish grey silty clay with reddish brown patches, LI = 0.314	61 80	m &		$c_u = 1.5 \text{ t/m}^2$ $c_u = 4.0 \text{ t/m}^2$	52.5 50.0	m,=1/(42N)m²/t	
1.40m to 2.00m 2.00m to 2.90m 2.90m to 3.70m 3.70m to 4.50m 4.50m to 5.50m	Yellowish grey and brownish sing clay, LI—U.LD2 Brownish clayey silty fine to medium sand / sandy silty clay Greyish brown dirty fine to coarse sand with weathered stones Yell grey clayey silty fine to coarse sand with weathered stones (wdr.) Yellowish grey highly / completely weathered fractured rock Greyish brown & grey completely weathered severely jointed rock	24 74 ×100 RB	24 70 100 200	φ = 32° φ = 40° φ = 42°	c. = 100 t/m²		C using q_e^{\pm} 22 N t/m^2 C using q_e^{\pm} 26 N t/m^2 C using q_e^{\pm} 26 N t/m^2 C using q_e^{\pm} 35 N t/m^2	, 1
6.50m to 8.50m	Brownish and grey highly weathered severely jointed rock	09						

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				to the factor of	Shear Strength	% 5	Compressibility	
Depth	700	z	Design N	Design N Angle of Hickory	ටී		A STATE OF THE STA	ŧ
Below GL	2011					45.5		
0.00m to 0.60m 0.60m to 1.40m	Br grey slity clay with brown & black patches, LI = 0.215 Yellowish grey soft slity clay with reddish brown patches, LI = 0.45	0 0	2 4		$c_u = 1.0 \text{ t/m}^2$ $c_u = 0.75 \text{ t/m}^2$	44.7 28.1	C using 0 = 24 N t/m ²	
1.40m to 2.40m 2.40m to 4.00m 4.00m to 5.50m 5.50m to 6.70m	Greyish soft say day man coarse sand weathered stones Brownish grey completely weathered / highly weathered fractured rock Brownish highly weathered severely jointed rock (siltstone)	31,44 >100 RB	32 200	φ = 34° φ = 42°	$\omega_{\rm r} = 100 \rm t/m^2$		C using $q_e = 28 \text{ N t/m}^2$ C using $q_e = 35 \text{ N t/m}^2$	1
6.70m to 7.50m	Light brownish and light grey widely jointed hard rock (siltstone)							
Boret	Borehole BH20 (GL = 1.250m RL)							ı
Cooth		Z	Design N	Angle of friction	Shear Strength	P %	Compressibility	I
Below GL	Soil					42.9		
0.00m to 0.60m 0.60m to 1.40m	Yellowish grey silty clay, $Ll = 0.249$ Light grey very soft silty clay with reddish brown patches, $Ll = 0.431$.	0 10	4 4		$c_u = 0.75 \text{ V/m}^2$ $c_u = 5.0 \text{ V/m}^2$	48.0	m _v =1,/(42N)m²/t	
1.40m to 2.60m 2.60m to 3.40m 3.40m to 4.80m	Brownish grey silty clay with graver and send, Lindous by Company Yellowish grey clayey silty fine to coarse sand with weathered stones yellowish grey completely / highly weathered fractured rock	>50 RB	500	ф = 38°	$c_{\rm u}=100~{\rm t/m^2}$		C using q₀= 25 N Vm² C ự sing q₀= 35 N V/m²	
4.80m to 6.20m	Light brownish grey weathered closely jointed rock Light brown and grey widely jointed hard rock (siltstone)							
Bore	Borehole BH21 (GL = 1.354m RL)							
					Shear Strength	2	Compressibility	

Denth		z	Design N	Design N Angle of friction	Shear Strength pl % Compressibility cu	8 년	Compressibility
Below GL	Soil				1	46	
0.00m to 0.60m	Yellowish grey medium stiff silty clay, $Ll = 0.083$	·	C		$c_u = 1.5 \text{Um}^2$	56.8	
0.60m to 1.40m	Yellowish grey soft silty clay with yellow patches, LI = 0.299	V 1	, ,		$c_u = 3.5 \text{ t/m}^2$		
1.40m to 1.90m	Lt grey soft silty clay with reddish brown patches	~			$c_u = 6.0 \text{ t/m}^2$	31.2	m _v =1/(48N)m²/t
1.90m to 2.30m	Yell brown and grey sandy silty clay with gravel , $Ll = 0.099$		1 : i	÷ 37°			C using $q_c = 24 \text{ N t/m}^2$
2.30m to 4.00m	Yell grey clayey silty sand with sandy clay lumps and weathered stones	•	, C	¢ - €.			C using $q_c = 28 \text{N} \text{J/m}^2$
4.00m to 4.50m	Yellowish grey dirty fine to coarse sand	O G	200	! -	$c_u = 100 \text{ J/m}^2$		C using $q_c=35~N~\text{t/m}^2$
4.50m to 5.50m	Yellowish grey highly weathered fractured rock	ž	20				
5.50m to 8.10m	Greyish weathered severely jointed rock						
21 810mto 8.50m	Brownish & grey weathered closely jointed rock						
اد							

GL = 1.267m RL
BH22
hole
30re

			1	Andle of friction	Shear Strength	% Id	Compressibility
Depth		z	Design in		3		
Below GL	Soli	c,	3		cu = 1.5 t/m ²	54.1	
0.00m to 1.30m 1.30m to 2.60m	Yellowish grey silty clay, $LI = 0.24$ Dark grey soft clay with reddish brown patches, $LI = 0.509$	000	ਜ ਜ		$c_u = 0.75 \text{ t/m}^2$ $c_u = 0.75 \text{ t/m}^2$	73.8	
2.60m to 3.40m 3.40m to 4.00m	Black organic sandy clay Dark greenish grey dirty fine to medium sand	17 >50	18 60	φ = 32° φ = 38°			C using $q_c = 22 \text{ N t/m}^2$ C using $q_c = 28 \text{ N t/m}^2$
4.00m to 4.80m 4.80m to 5.60m	rn weathered athered stone	>100 RB	100	φ = 42°	$c_u = 100 \text{ t/m}^2$		C using $q_c=30 \text{ N t/m}^2$ C using $q_c=35 \text{ N t/m}^2$
5.60m to 6.70m 6.70m to 9.10m	Brownish grey highly weathered tractured fork Brownish and grey highly weathered severely jointed rock Br and grey weathered closely jointed rock						
Boreho	Rorehole BH23 (GL = 1,200m RL)						
Denth		2	Design N	Angle of friction	Shear Strength Cu	я %	Compressibility
Below GL	Soil					43.4	
0.00m to 0.60m 0.60m to 2.20m	Yellowish grey silty clay, Ll $*0.136$ Light brownish grey soft silty clay with yellow patches, Ll = 0.435 to 0.911	° 0	4 0		$c_u = 0.75 \text{ t/m}^2$ $c_u = 1.0 \text{ t/m}^2$	68-74 43.2	
2.20m to 3.50m 3.50m to 4.60m	Dark grey very soft silty clay with medium sand patches and decayed wood Dark yellowish grey dirty fine to coarse sand weathered stones	100	75	φ = 40°	c _u = 75 t/m²		ೆ usinુ Ç= 28 N t/m² C using q= 30 N t/m²
4.60m to 5.50m 5.50m to 6.30m	Dark yellowish grey completely weathered fractured rock Yellowish grey highly weathered fractured rock	ALOU, NB RB	200		$c_u = 100 \text{ t/m}^2$		C using q_c = 35 N t/m^2
6.30m to 8.30m	Brownish and grey weathered severely jointed rock						
Boreh	Borehole BH24 (GL = 1.295m RL)		wa				The state of the s
Depth	Soil	Z	Design N	Angle of friction	Shear Strength	% Id	Compressibility
0.00m to 0.50m	Yellowish grey silty clay, LI = 0.046	c	< 1		$c_u = 0.75 \text{ t/m}^2$		
0.50m to 1.80m	Light brownish grey soft silty clay with few stones, $Ll = 0.544$. 0	l vi		$c_u = 0.50 \text{ t/m}^2$	60.1	
1.80m to 2.40m	Light grey soft silty clay, LI = 1.0 /	>50	90	⊕ # 38°	•		C using q= 26 N Vm²
2,40m to 2.80m	Yell grey dirty lille to coarse can't man man and man	RB	200		$c_u = 100 \text{ t/m}^2$		in A in Co Lon Billish o

Light grey and light brown weathered severely jointed rock

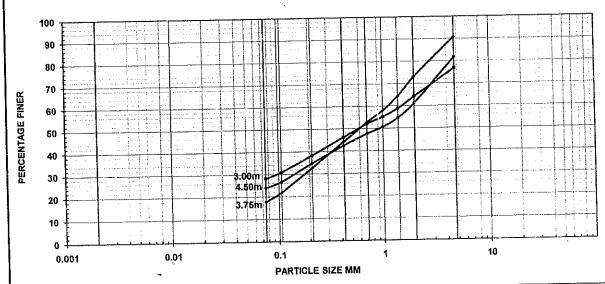
Yellowish grey highly weathered fractured rock

2.80m to 3.40m 3.40m to 5.40m

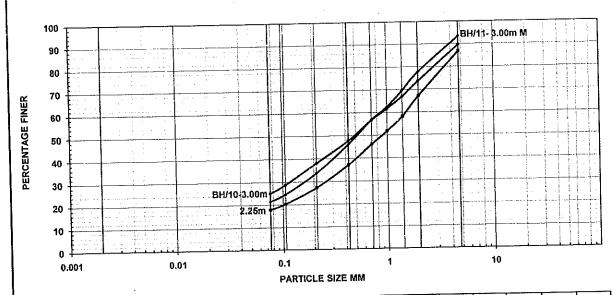


PROJECT:

Residential Building, Mogapair



BH NO DEPTH	PER	CENT	AGE F	INER (ize in m	m)	Fine Gravel	Sand	Medium Sand MS	Fine Sand FS	Silt	Clay	Classifi cation CLASS	D50 mm	cu (sand)	cc (sand)
BH/9 3.00m BH/9 3.75m BH/9 4.50m	1	20 00.0 00.0 00.0	4.75 76.9 90.8 81.8	2 64.3 73.1 61.3	0.43 46.3 44.3 42.6	0.08 28.2 17.7 24.0	0	23.1 9.2 18.2	12 6 17.7 20.5	18.0 28.8 18.7	18.1 26.6 18.6	28 17 24	7.7	GCS GC-SP GC-SW	0.586 0.597 0.921	14.684 11.381 14.936	0.860 0.670 1.086



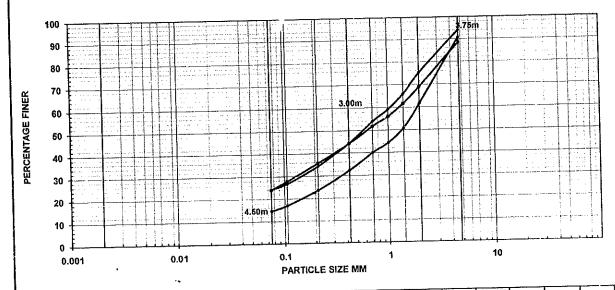
вн по	DEPTH	PE	RCENT	AGE F	INER (Sieve s	ize in n	1FB)	Fine Gravel	Coarse Sand	Medium Sand	Sand	Silt	Clay	Classifi cation	D50 mm	cu (send)	cc (sand)	
Britis	М	80	20	4.75	2	0.43	0.08	0	G	CS	MS	FS	Si	 '.9	GC-SP	0.892	10.701	0.890	l
BH/10	2.25m		100.0	86.9	67.2	37.2	17.9		13.1 6.5	19.7 15.7	30.0 31.7	19.3 24.6		1.5	SC-SP	0.512	8.842	0.795	L
BH/10 BH/11	3,00m 3,00mM		100.0	89.7	73.8	46.1	21.5 25.0		10.3	15.9	28.1	22.7	25	i.0	GCS	0.485	11,729	0.767	F
DENT	3.00111101		100.0															Y :	ť

SECTECHNICAL Solutions, Chennal

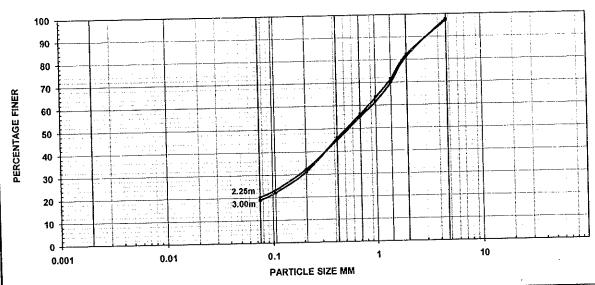
GRAIN SIZE DISTRIBUTION CURVES

PROJECT:

Residential Building, Mogapair



BH NO	DEPTH	PE	RCENT	AGE F	INER (Sieve s	ize in π	ım)	Gravel	Sand	Medium Sand	Sand	Siit	Clay	Classifi cation CLASS	D50 mm	cu (sand)	cc (sand)
BH/12 BH/12 BH/12	M 3.00m 3.75m 4.50m	80	20 100.0 100.0 100.0	4.75 88.5 94.0 90.7	2 69.0 75.2 61.7	0.43 44.3 44.4 32.4	0.0B 24.0 24.2 14.6	0	G 11.5 6.0 9.3	19.5 18.8 29.0	MS 24.7 30.8 29.3	FS 20.3 20.2 17.8	24	1.0 1.2 1.6	GCS SC-SP GC-SW	0.528 0.575 1.335	13.751 9.605 10.975	0.845 0.871 1.169
DIV12	4.5011		100.0									<u> </u>	<u> </u>		1			



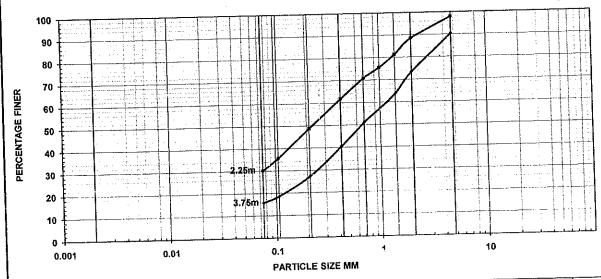
вн по	DEPTH	PERCE	NTAGE F	INER (Sieve s	ize in n	nm)	Fine Gravel	Sand	Medium Sand	Sand	Silt	Clay	Classifi cation CLASS	D50 mm	cu (sand)	cc (sand)
BH/13	M 2.25m	80 20 100	4.75 0 97.3	2 82.2	0.43 45.9	0.08 19.0	0	G 2.7	15.1	MS 36.3	FS 26.9 24.7		9.0 0.4	SC-SP SC-SP	0.521 0.545	7.669 8.359	0.770 0.819
BH/13	3.00m	100	0.88	81.4	45.1	20.4		2.0	16.6	36.3			<u></u>	000:			

EOTECHNICAL Solutions, Chennal

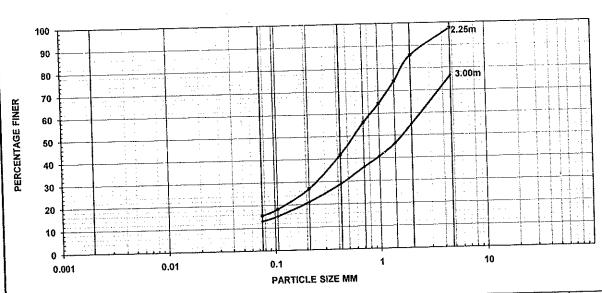
GRAIN SIZE DISTRIBUTION CURVES

PROJECT:

MIG, Perambakkam



BH NO DEPTH	PERCENTAGE FINER (Sleve size in mm)	Fine Gravel	Sand	Medium Sand	Sand	Sill	Clay	Classifi cation CLASS	D50 mm	cu . (sand)	cc (sand)	
BH/14 2.25m BH/14 3.75m	80 20 4.75 2 0.43 0.08 0 100.0 98.0 88.5 61.8 30.2 100.0 90.5 73.5 40.5 15.8	9.5	9.5 17.0	MS 26.7 33.0	FS 31.6 24.7	SI 30 15	5.8	SC-SP GC-SP	0.226 0.670	6.717 9.308	0.648 0.752	



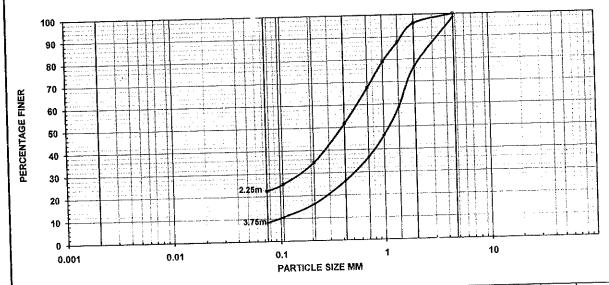
BUND	DEPTH	PE	RCENT	AGE F	INER (Sieve s	ize in m	nm)	Fine Gravel	Coarse Sand	Medium Sand	Sand	Silt	Clay	Classifi cation	D50 mm	cu (sand)	cc (sand)	
BH NO	М	80	20	4.75	2	0.43	80.0	0	G	CS	MS 44.0	FS 26.3	Si 1	C 5.5	CLASS SC-SP	0.572	6.377	0.932	
BH/15	2.25m		100.0	97.6 76.6	85.8 55.0	41.8 28.9	15.5 13.0		23.4	11.8 21.6	26.1	15.9	1	3,0	GC-SW	1.617	10.970	1.425	r
BH/15	3,00m		100.0	70.0								<u> </u>		<u> </u>				£ v 88	ľ
				<u> </u>	ļ	<u> </u>	<u> </u>	 	·	ļ	 	 	\					<u>/</u>	1

SECTECHNICAL Solutions, Chennal

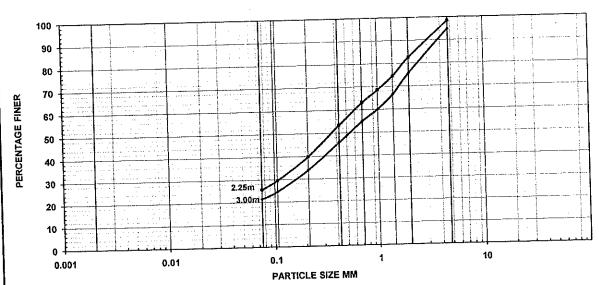
GRAIN SIZE DISTRIBUTION CURVES

PROJECT:

MIG, Perambakkam



	ОБЕТН	PE	RCENT	AGE F	INER (Sieve s	ize in m	nm)	Fine Gravel	Coarse Sand	Medium Sand	Fine Sand	Silt	Clay	Classifi cation	D50 mm	cu (sand)	cc (sand)	
BH NO	DEPTH M 2,25m	80	20 100.0	4.75 100.0	2 96,1	0 43 51.7	0.08 22.5	0	G	CS 3.9	MS 44.4	FS 29.2	1	C 2.5 ,3	SC-SP SW	0.397	4.813 6.720	0.978	
BH/16			100.0	98.5	76.9	26,4	8.3		1.5	21.6	50.5	18.1							
 															1	<u> </u>	l	L	J



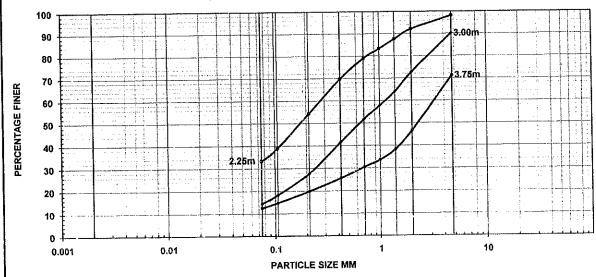
										Fine	Coarse	Medium	Fine	Silt	Clay	Classifi	D50	cu	cc
l l	H NO	DEPTH	PEI	RCENT	AGE F	INER (Sieve s	ize in n	nm)	Gravel	Sand	Sand	Sand	Sill	Clay	cation CLASS	mm	(sand)	(sand)
ΙL		М	80	20	4.75	2	0.43	0.08 25.7	0	G 1,6	CS 15.8	MS 29.2	FS 27.7	2!	5.7	SC-SP	0.357	8.152	0.696
	3H/17 3H/17	2.25m 3.00m		100.0	98.4 94.9	82.6 75.8	53.4 46.0	21.4		5.1	19.1	29.8	24.6	2	1.4	SC-CP	0.533	10,144	0.714
	3, 11, 11	0.00					<u> </u>							l		l			

SEOTECHNICAL Solutions, Chennal

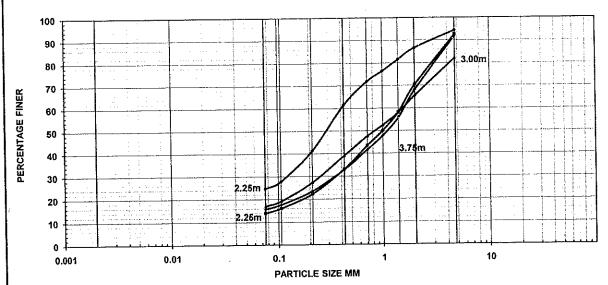
GRAIN SIZE DISTRIBUTION CURVES

PROJECT:

MIG, Perambakkam



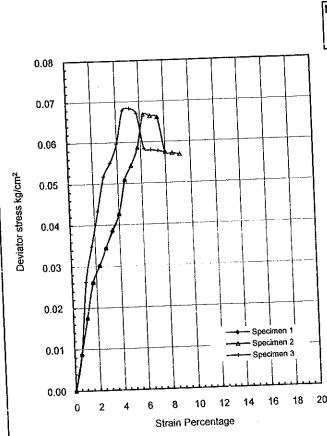
вн по	DEPTH	PE	RCENT	AGE F	INER (Sieve s	ize in m	m)	Fine Gravel	Coarse Sand	Medium Sand	Fine Sand	Silt	Clay	Classifi cation	D50 mm	cu (sand)	cc (sand)
	М	80	20	4.75	2	0.43	0.08	D	G	CS	MS	FS	Si	C	CLASS			
BH/18	2.25m		100.0	98.2	92.1	69.8	33.3		1.8	6.1	22.3	36.5	33	3.3	SC-SP	0.175	4.668	0.717
					CALADON TO		14.5		9.7	17.5	31.2	27.1	14	1.5	GC-SP	0.646	10.048	0.696
BH/18	3.00m		100.0	90.3	72.8	41.6								2.6	GS-SW	2.246	10.786	3.046
BH/18	3.75m		100.0	71.3	46.7	25.7	12.6		28,7	24.6	21.0	13.1			03-044	2,240	10.700	
	1					1					l		l		1			
			1						1					<u> </u>	<u> </u>		<u> </u>	



вн по	DEPTH	PE	PERCENTAGE FINER (Sieve size in mm)							Coarse Sand	Medium Sand	Fine Sand	Silt	Clay	Classifi cation	D50 mm	cu (sand)	cc (sand)
	M	80	20	4.75	2	0.43	0.08	0	G	CS	MS	FS	Si	С	CLASS			0004
BH/19	2.25m		100.0	92.7	70.5	33.1	14.0		7.3	22.2	37.4	19.1	14	1.0	SC-SW	0.995	8.068	0.934
BH/19	3.75m		100.0	92.1	68.3	32.9	15.7		7.9	23.8	35.4	17.2	1:	5.7	SC-SW	1.092	8.554	1.103
BH/20	2.25m		100.0	94.5	86.8	61.5	24.7		5.5	7.7	25.3	36.8	24	1.7	SC-SP	0.286	4.828	0.794
BH/20				82.3	65.7	39.1	17.0		17.7	16.6	26.6	22.1	1	7.0	GC-SP	0.837	11.585	0,691
BH/ZU	3,00m		100.0	04.5	00.7	35.1	17.0		 ''''	10.0			1	1				

ANNEXURE U1

Unconfined Compression Strength Test UCC on soil sample



Project:

MIG Perambakkam, M Block

27-Mar-13 Date of Test **BH/24** Borehole 1.50m Depth

Soil

Light yellowish grey silty clay with brown patches

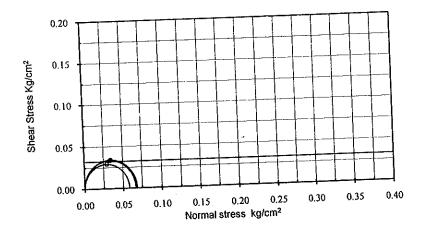
Insitu bulk density Insitu Dry Density Water Content	1.460 gm/cc 0.786 gm/cc 85.69 %
Liquia Limit %	83.30
Plastic Limit %	23.20
1 10000	00.40

60.10 Plasticity Index % 1.04 Liquidity Index

Maximum Shear Stress

Maximum Shear Siress									
Deviator stress	Shear stress kg/cm²								
0.058	0.029								
0.067	0.033								
0.068	0.034								
	Deviator stress 0.058 0.067								

Results Unconfined compression strength q _u Undrained Cohesion c _u Secant Modulus (undrained)	0.064 kg/cm² 0.032 kg/cm² 1.61 kg/cm²

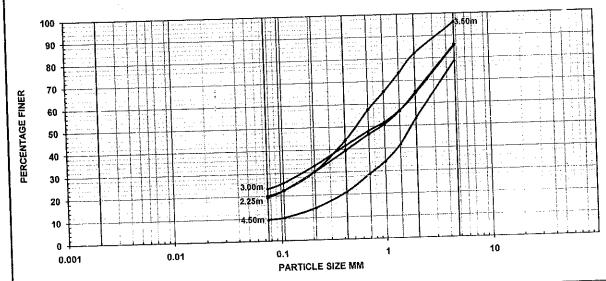




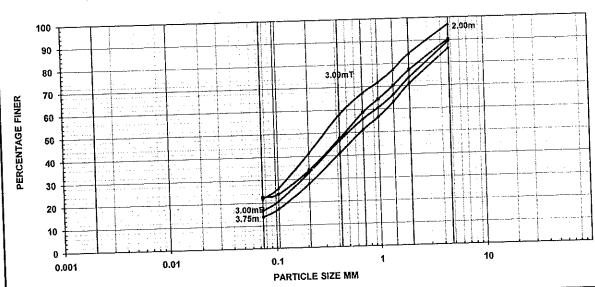
GRAIN SIZE DISTRIBUTION CURVES

PROJECT:

MIG, Perambakkam



									Fine	Coarse	Medium	Fine	Silt	Clay	Classifi	D50	cu	cc
21110	DEPTH	PE	PERCENTAGE FINER (Sieve size in mm)					Gravel	Sand	Sand	Sand		Ciay	cation CLASS	mm	(sand)	(sand)	
BH NO	М	80	20	4.75	2	0.43	0.08	0	G 14.2	CS 20.9	MS 25.4	FS 20.1	Si 19	.4	GCS	0.938	13.022	0.929
BH/21	2.25m		100.0	85.5	64.9 64.3	39.5 41.6	19.4 23.2		14.5	21.2	22.7	18.4	23		GCS	0.854	13.104 6.431	0.978
BH/21 BH/22	3.00m 3.50m		100.0	96.1	82.3	43.9	20.1		3.9	13.8	38.4	23.8).1 ,5	SC-SP GSW	1.807	7.420	1.547
BH/22	4.50m	~	100.0	78.8	53.3	21.1	9.5		21.2	25,5	32,2	11.0		Ľ			<u> </u>	
			<u>L.</u>	<u> </u>		<u></u>	L			<u> </u>								



r	_ -				WED 16		zo in m	·m)	Fine		Medium		Sill	Clay	Classifi	D50	cu	cc (sand)
вн ио	DEPTH	80	20	4.75	NER (S	0.43	80.0	0	Gravel G 9,6	Sand CS 13.2	Sand MS 29.6	Sand FS 25.1	Si 2:	C 2.5	CLASS SC	mm 0.474	(sand) 7.867	0.704
BH/23	3,00mT 3,00mB		100.0 100.0	90.4 89.4 86.5	77.2 73.9 71.2	47.6 46.8 41.3	22.5 16.7 13.9		10.6 13.5	15.5 15.3	27.1 29.9	30.1 27.4	1	3.7 3.9	GC-SP GC-SP SC-SP	0,509 0,667 0,303	10.486 10.502 6.383	0.562 0.665 0.635
8H/23 BH/24	3.75m 2.00m		100.0	97.0	84.3	58.1	21.9		3.0	12.7	26.2	36.2	2	1.9	30-3F	0.303	0.000	

ANNEXURE CS1

Unconfined Compressive Strength Test on Rock Core Sample

Project:

TNSCB, MIG, Perambakkam

Date of Test

12-Apr-13

Borehole

BH/19

Depth

6.50m to 7.50m (S2)

Description

Light brown and light grey rock

Insitu bulk density

2.758 gm/cc

Insitu Dry Density

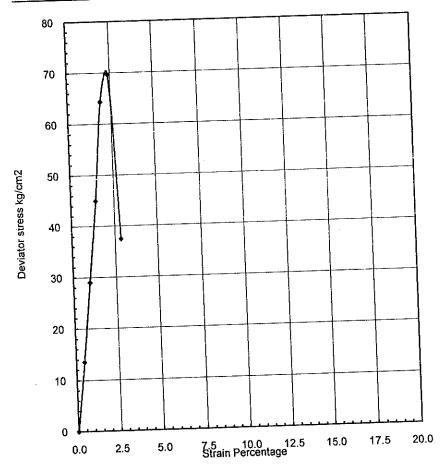
2.642 gm/cc

Water Content

4.41 %

Maximum Shear Stress

Maximum ones ones	-			
Specimen No:	Deviator stress	Shear stress kg/cm²		
Specimen 1	0.0	70.0		



Results

Unconfined compression strength qu

70.0 kg/cm²

Young's Modulus (secant)

3145 kg/cm²

ANNEXURE CS2

Unconfined Compressive Strength Test on Rock Core Sample

Project:

TNSCB, MIG, Perambakkam

Date of Test

12-Apr-13

Borehole

BH/20

Depth

5.80m to 6.80m (S1)

Description

Light brown and light grey rock

Insitu bulk density

2.477 gm/cc

Insitu Dry Density

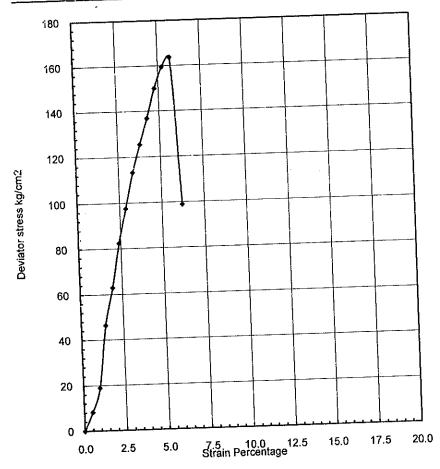
2.441 gm/cc

Water Content

1.48 %

Maximum Shear Stress

aximum Shear Stres	<u> </u>	
Specimen No:	Deviator stress	Shear stress kg/cm ²
Specimen 1	0.0	164.0



Results

Unconfined compression strength qu

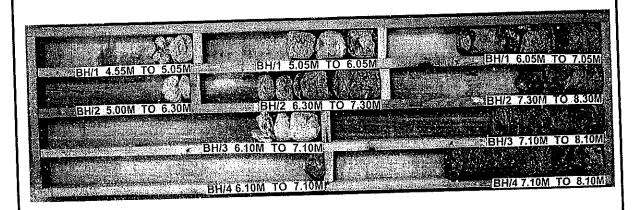
164.0 kg/cm²

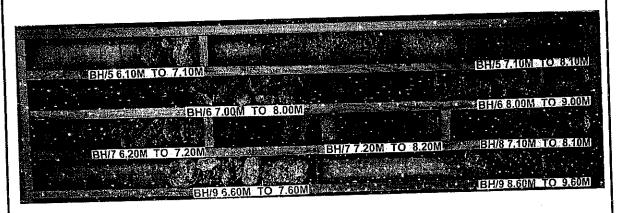
Young's Modulus (secant)

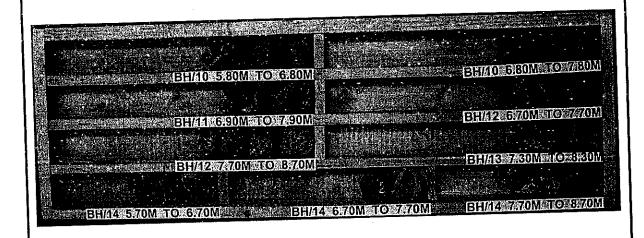
3242 kg/cm²

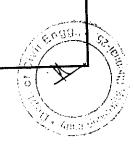


CORE SAMPLES FROM BH/1 to BH/14 MIG TENEMENTS, TNSCB, PERUMBAKKAM









CORE SAMPLES FROM BH/15 to BH/24 MIG TENEMENTS, TNSCB, PERUMBAKKAM

